

Lecture 4: Surface Parameterizations

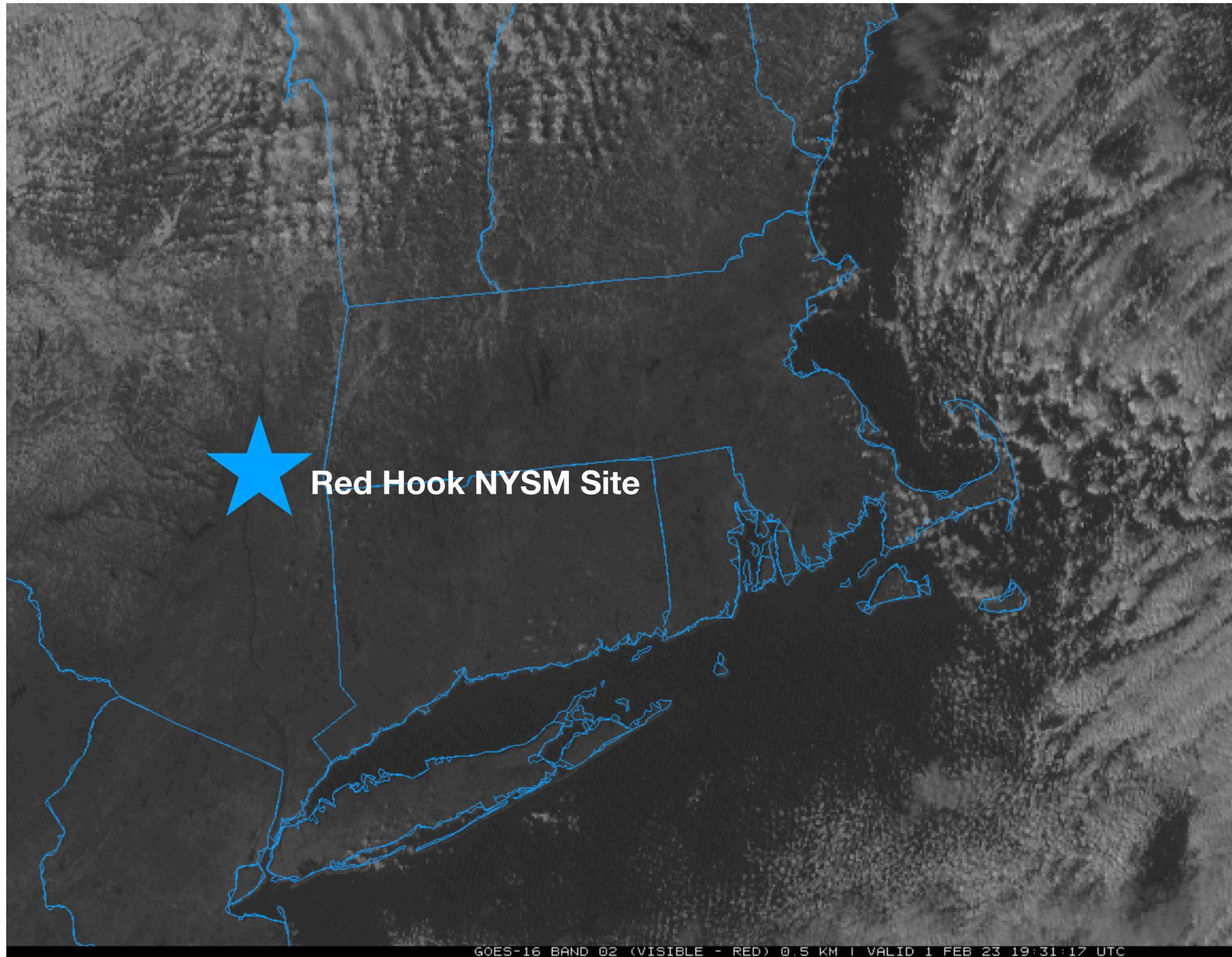
Announcements

- Homework on Boundary Layer Module
 - due: Monday Feb 6th
 - returned: Monday Feb 13th
 - questions on homework: by appointment
 - Readings: Stull Chapter 7
- Midterm exam: Monday March 6th

Today's Lecture

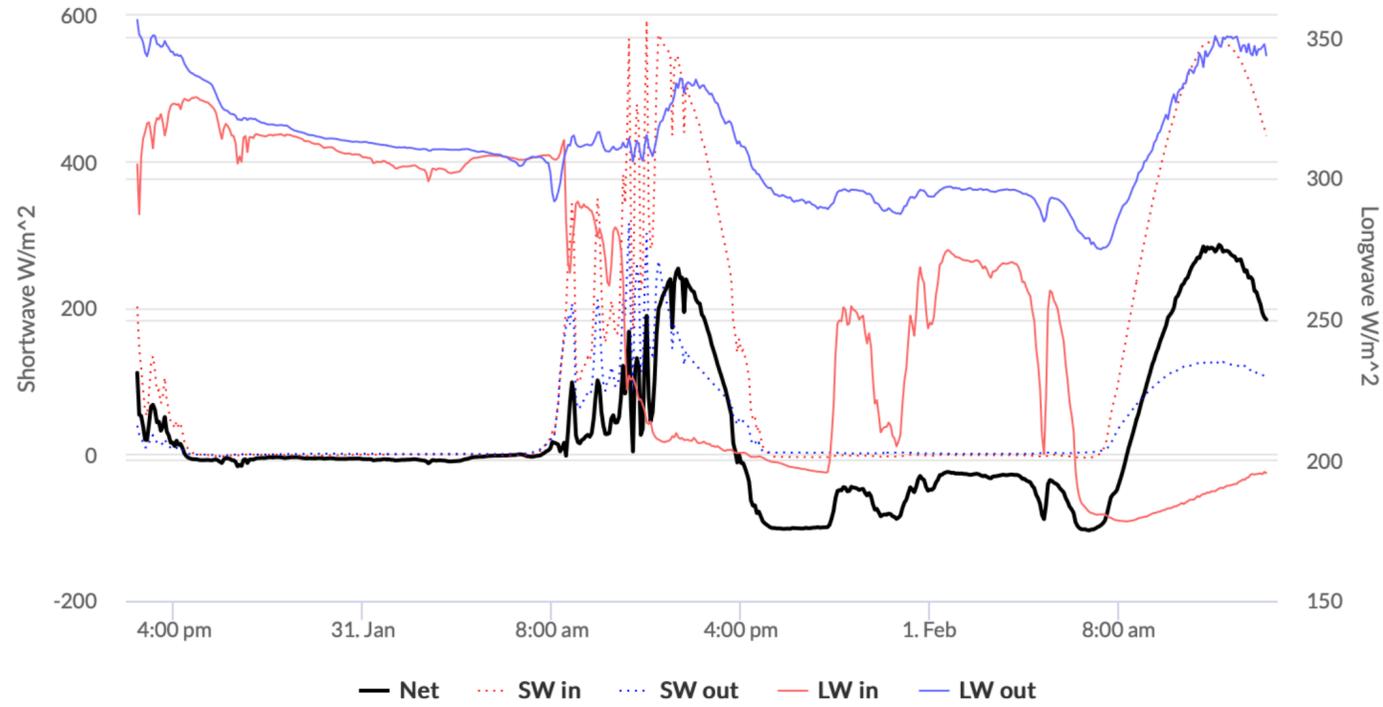
1. Bulk aerodynamic formulas
2. Drag coefficients, surface roughness
3. Energy Balance
4. NYS Mesonet—wind profiles

Today!

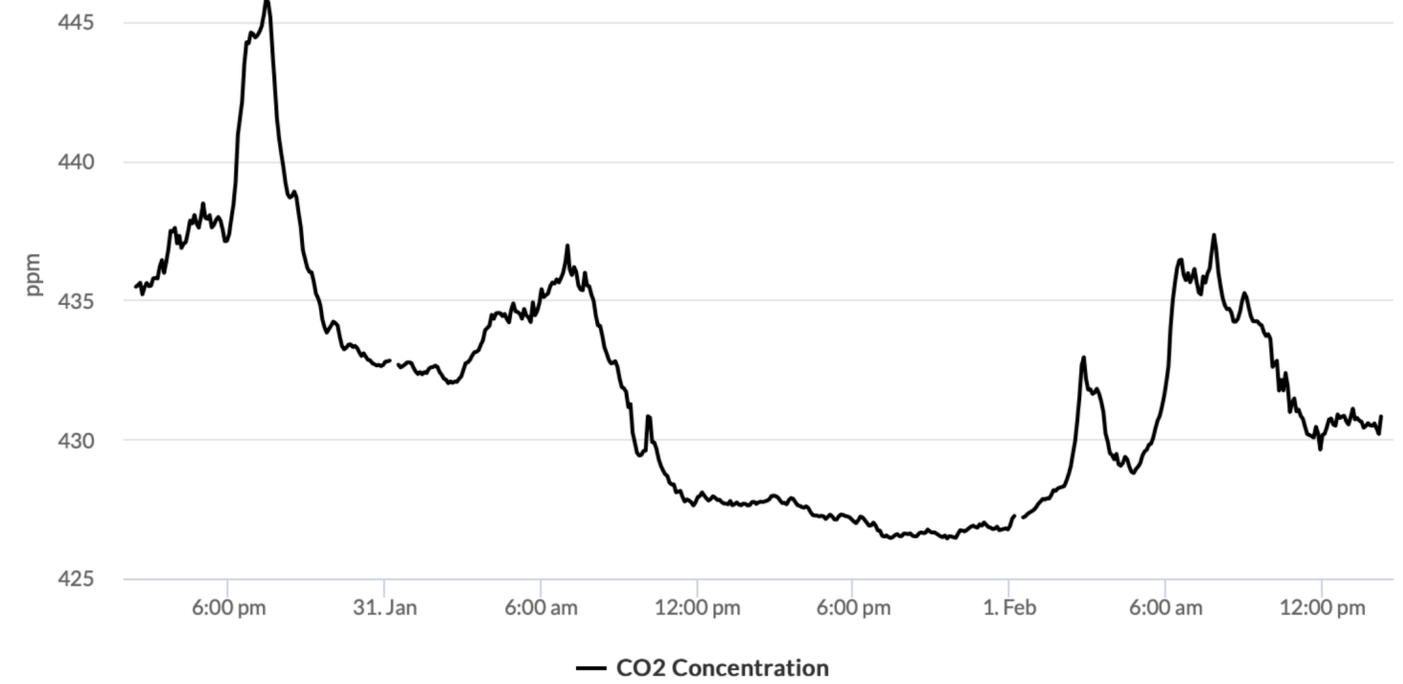


Today (and yesterday)!

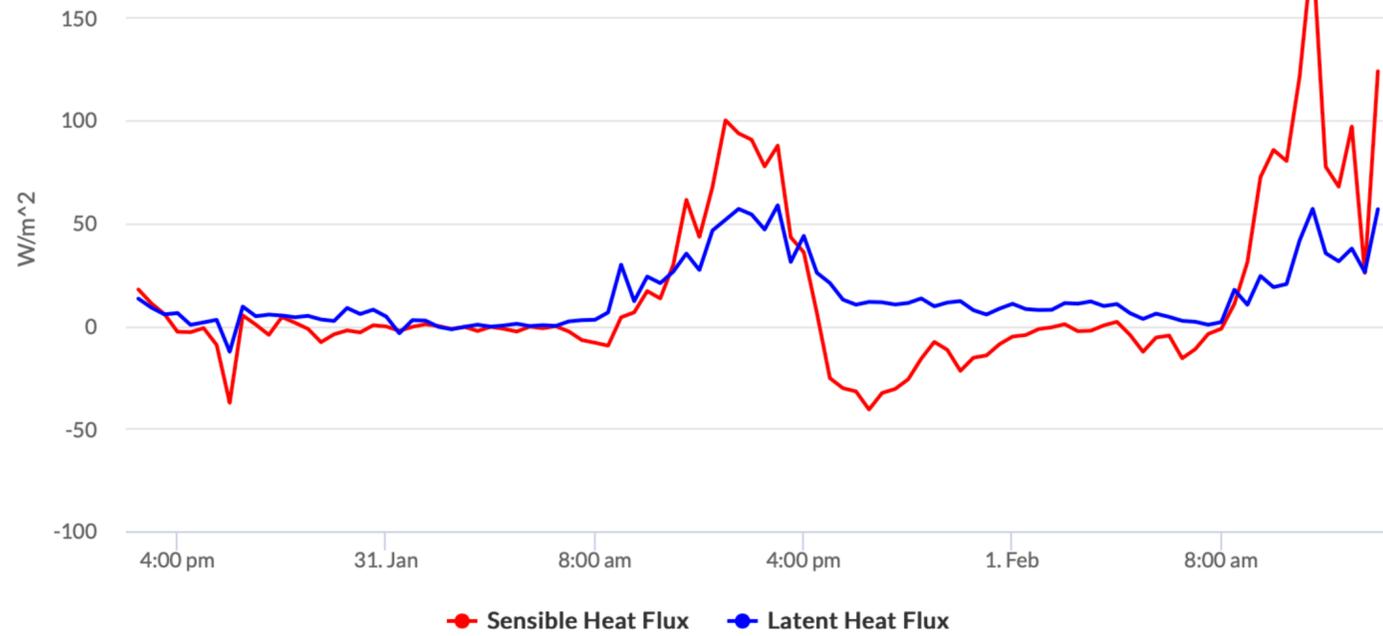
Red Hook - Net Radiation



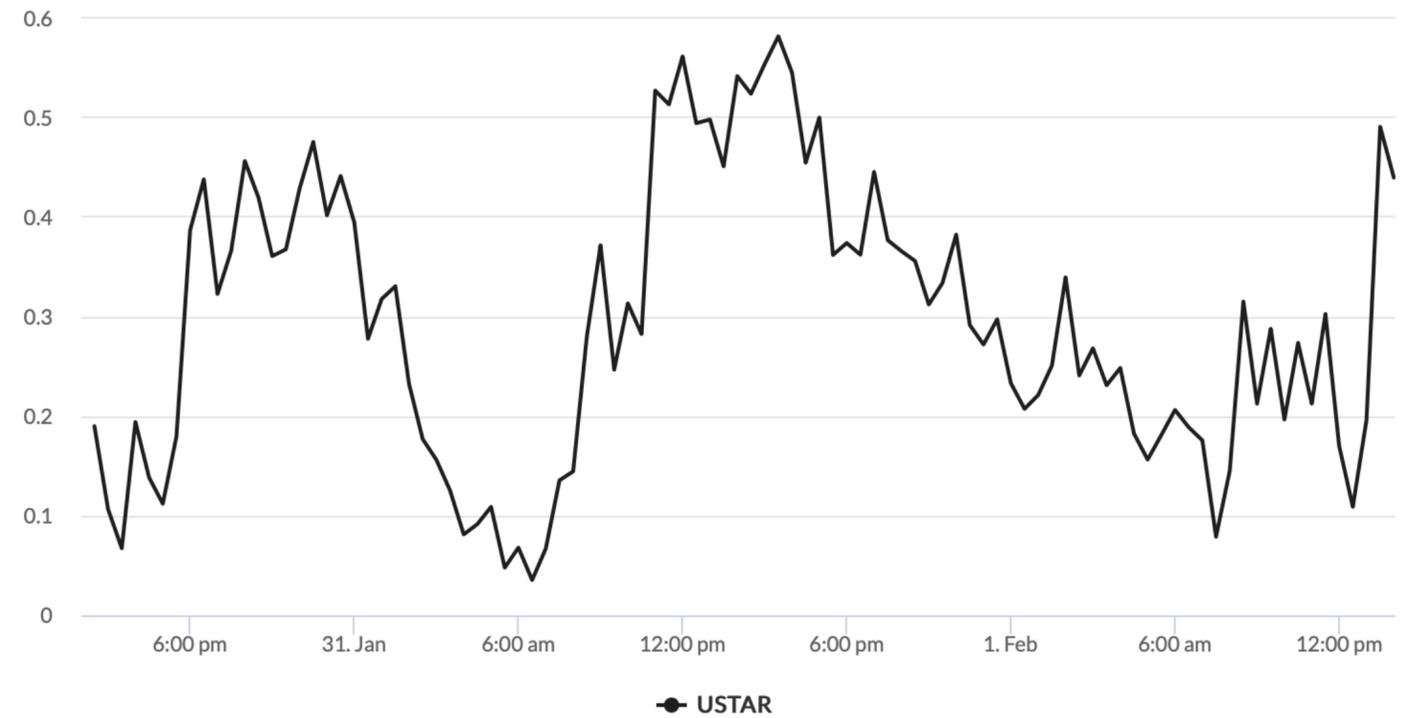
Red Hook - CO₂ Concentration



Red Hook - Heat Flux



Red Hook - USTAR

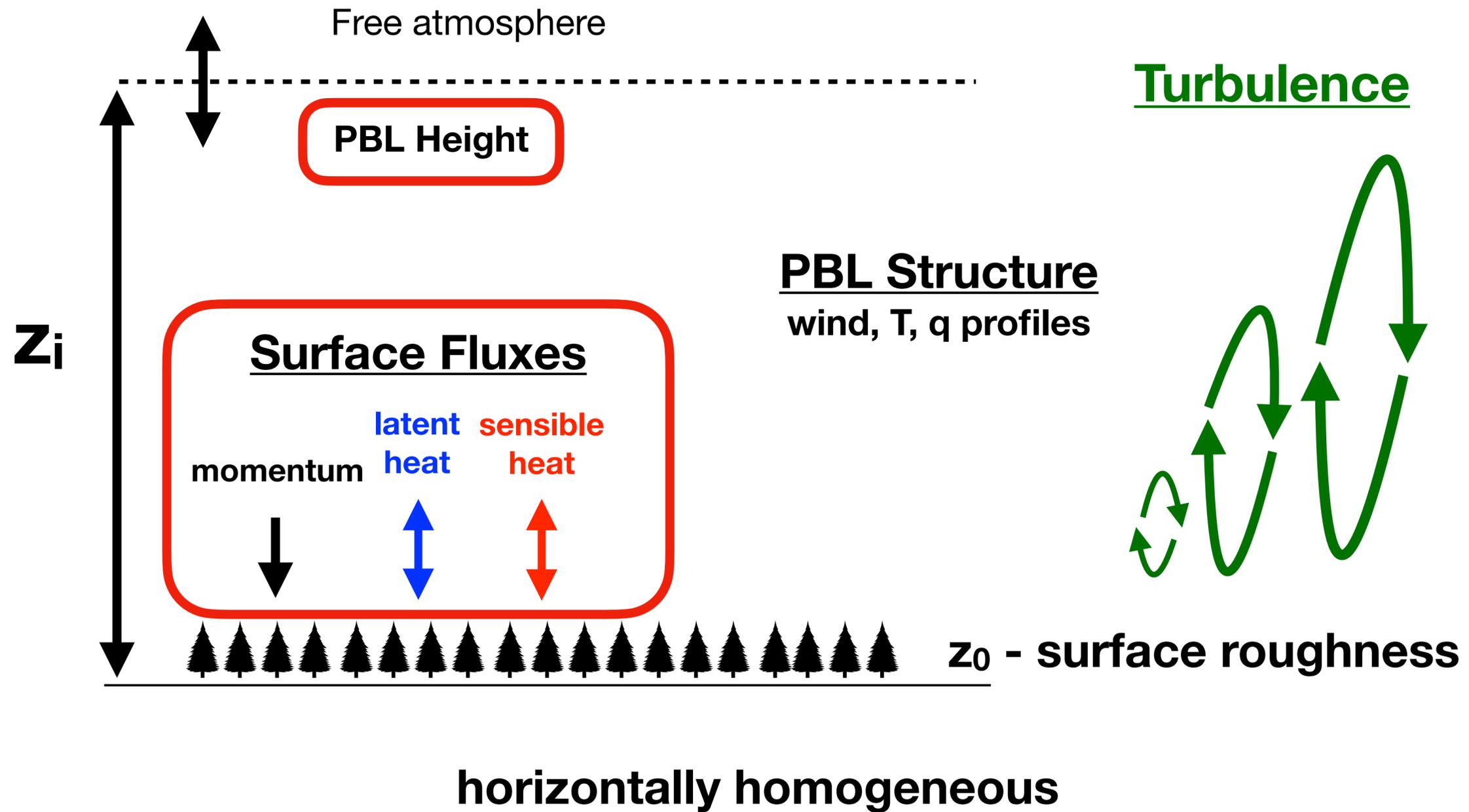


About that Problem Number 4....

Make sure you convert flux units (W m^{-2}) given
in the time series to kinematic units ($\text{ms}^{-1} \text{K}$)

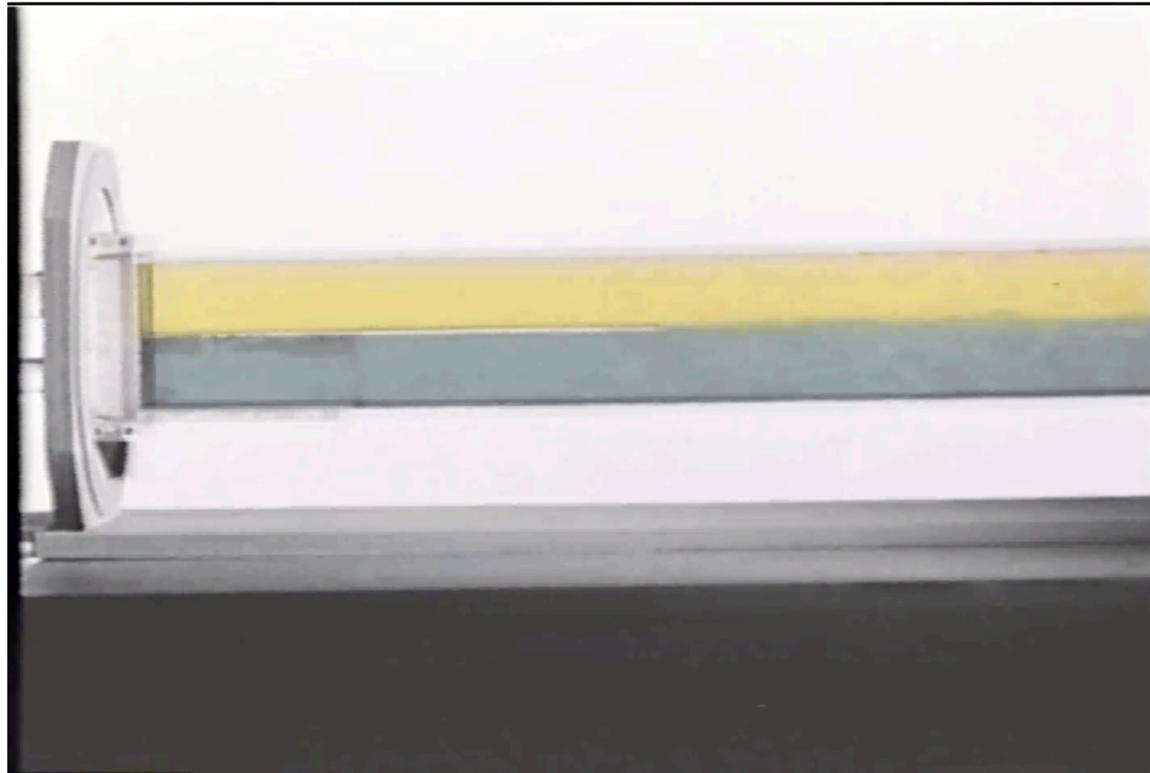
Hint: see Stull pages 47 -50!

Conceptual Model of the ABL

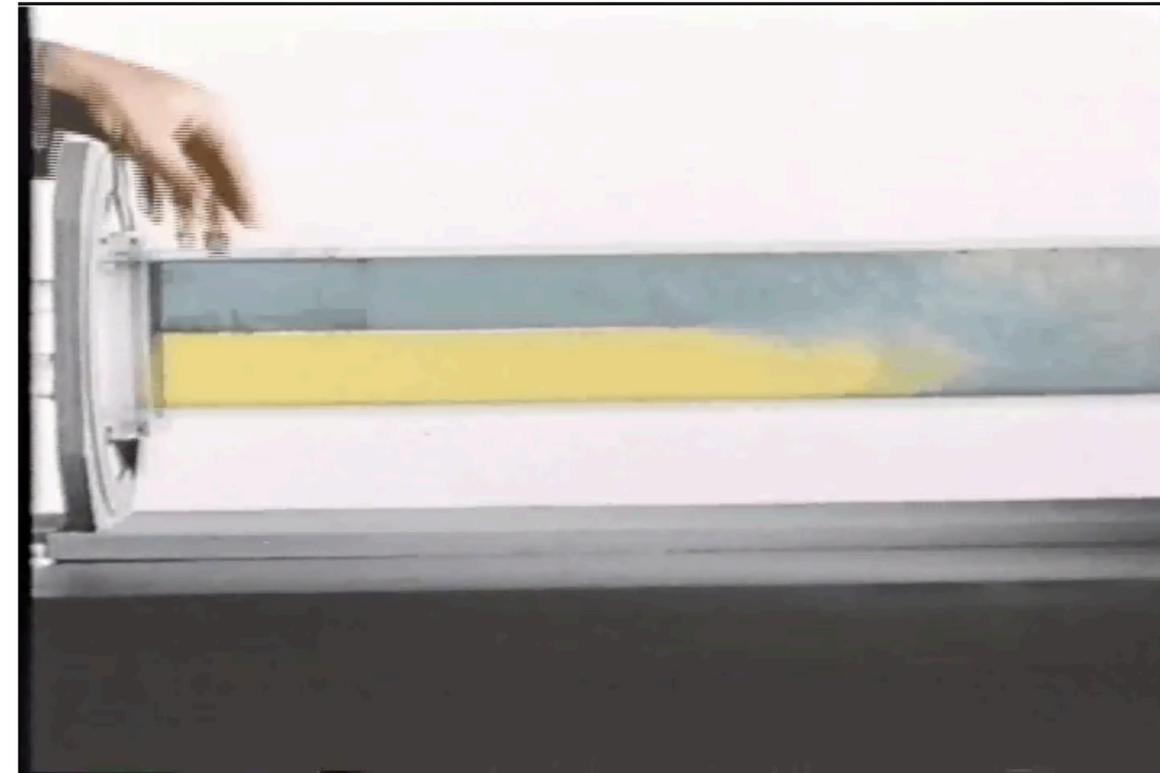


Stability enhances or suppresses turbulence (and fluxes)

Stable



Unstable



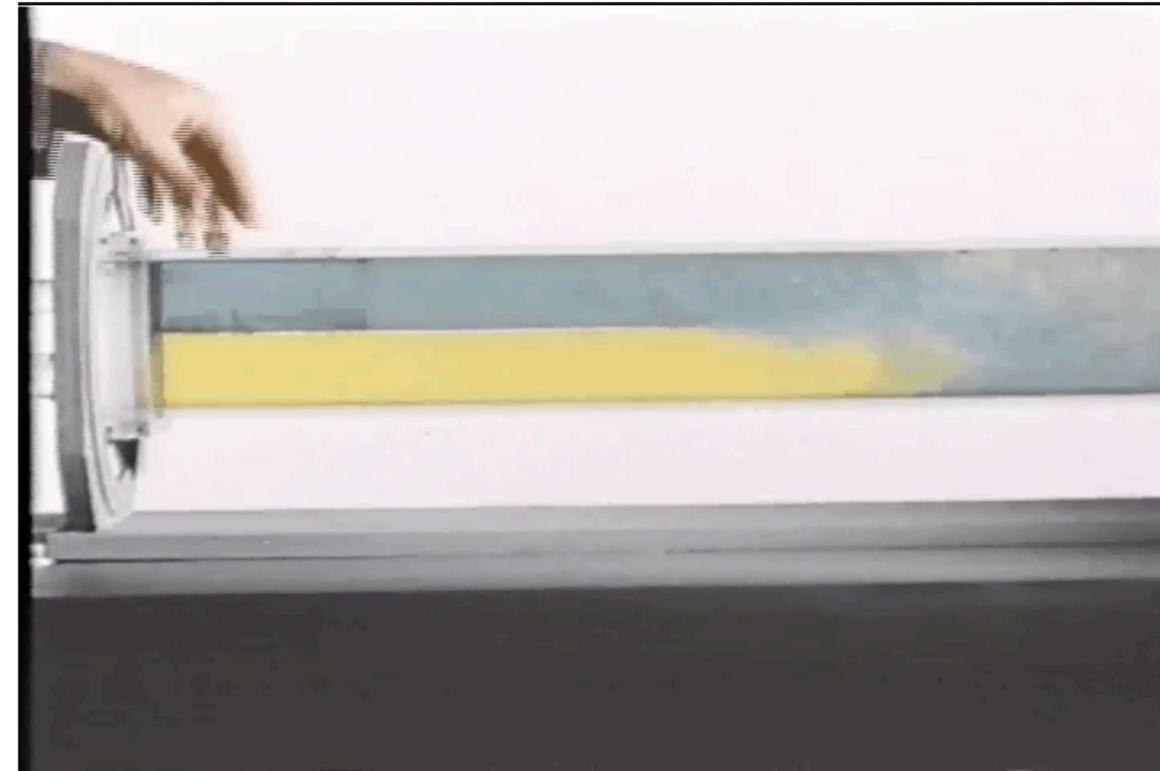
Turbulence, R.W. Stewart (1968)
Photos: J. Freedman

Stability enhances or suppresses turbulence (and fluxes)

Stable



Unstable



Turbulence, R.W. Stewart (1968)
Photos: J. Freedman

Stability enhances or suppresses turbulence (and fluxes)

Stable



Unstable



Turbulence, R.W. Stewart (1968)
Photos: J. Freedman

Stability Parameters

Gradient Ri

$$Ri = \frac{(g/\bar{\theta}_v) \partial \bar{\theta}_v / \partial z}{(\partial \bar{U} / \partial z)^2}$$

$$Ri \approx \frac{\text{buoyancy forcing}}{\text{shear forcing}}$$

- predicts turbulent/laminar flow
- applies any height in PBL

Obukhov Length

$$L = - \frac{\theta_v u_*^3}{g\kappa \overline{(w'\theta'_v)}_s}$$

$$L \approx - \frac{\text{shear forcing}}{\text{buoyancy forcing}}$$

- requires turbulence
- applies near-surface layer

Monin-Obukhov Similarity, z/L

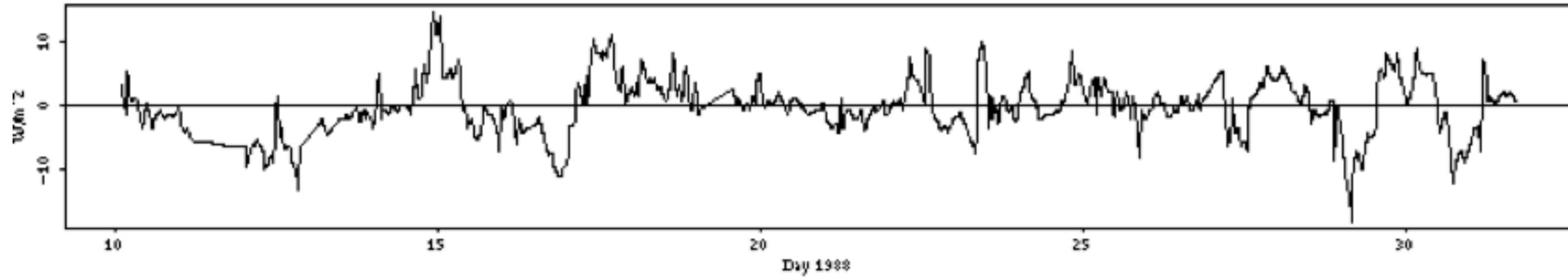
- MO Similarity accounts for relative importance of shear (mechanical turbulence) and buoyancy in the generation of turbulence and their effects on surface fluxes and surface layer profiles
- z = height above the surface
- ratio z/L is dimensionless
- can be described as a surface layer scaling parameter
- when z/L is small, buoyancy is less important
- as z increases, buoyancy increasingly important

Free Convection at the South Pole!

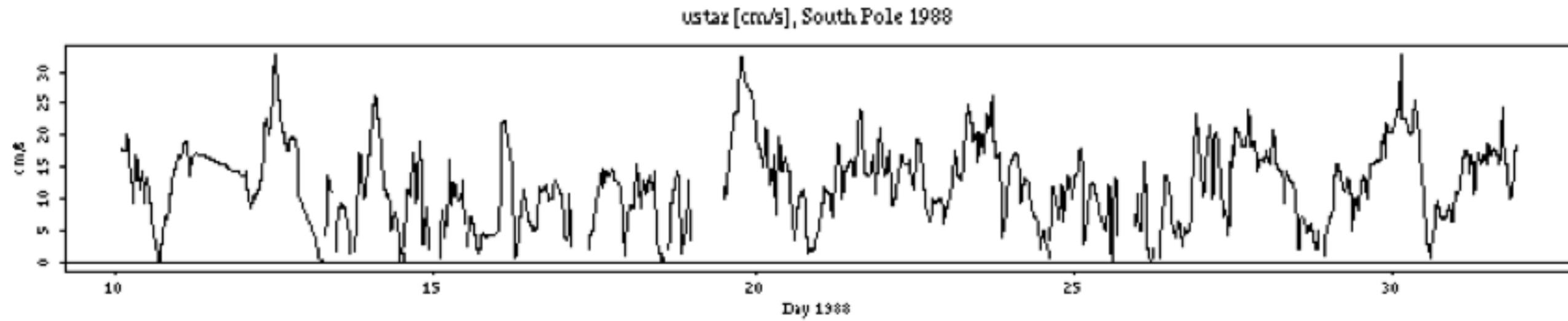
Courtesy of D. Fitzjarrald

sensible heat flux, South Pole 1988 Fitzjarrald & Martin W/m^2

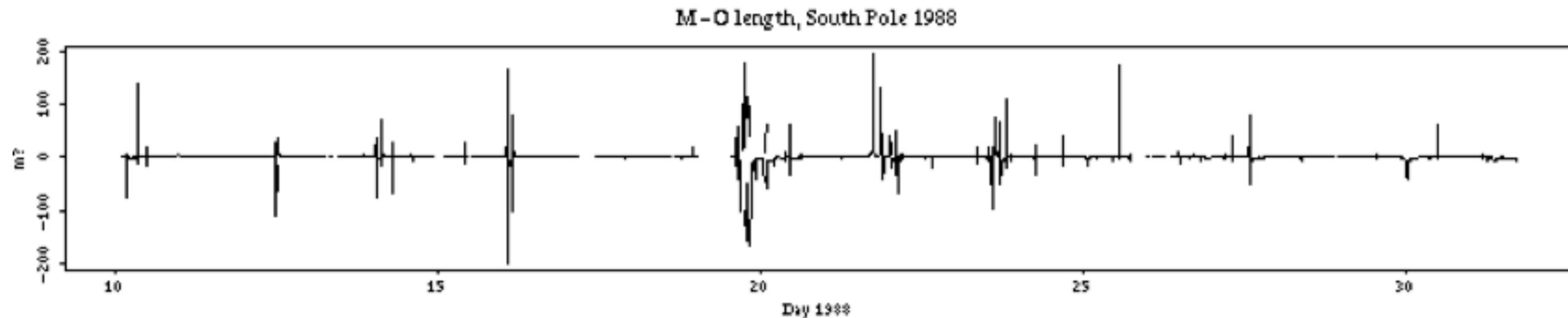
Heat
Flux



u_*



M-O
length
(L)



Law of the Wall

Neutral

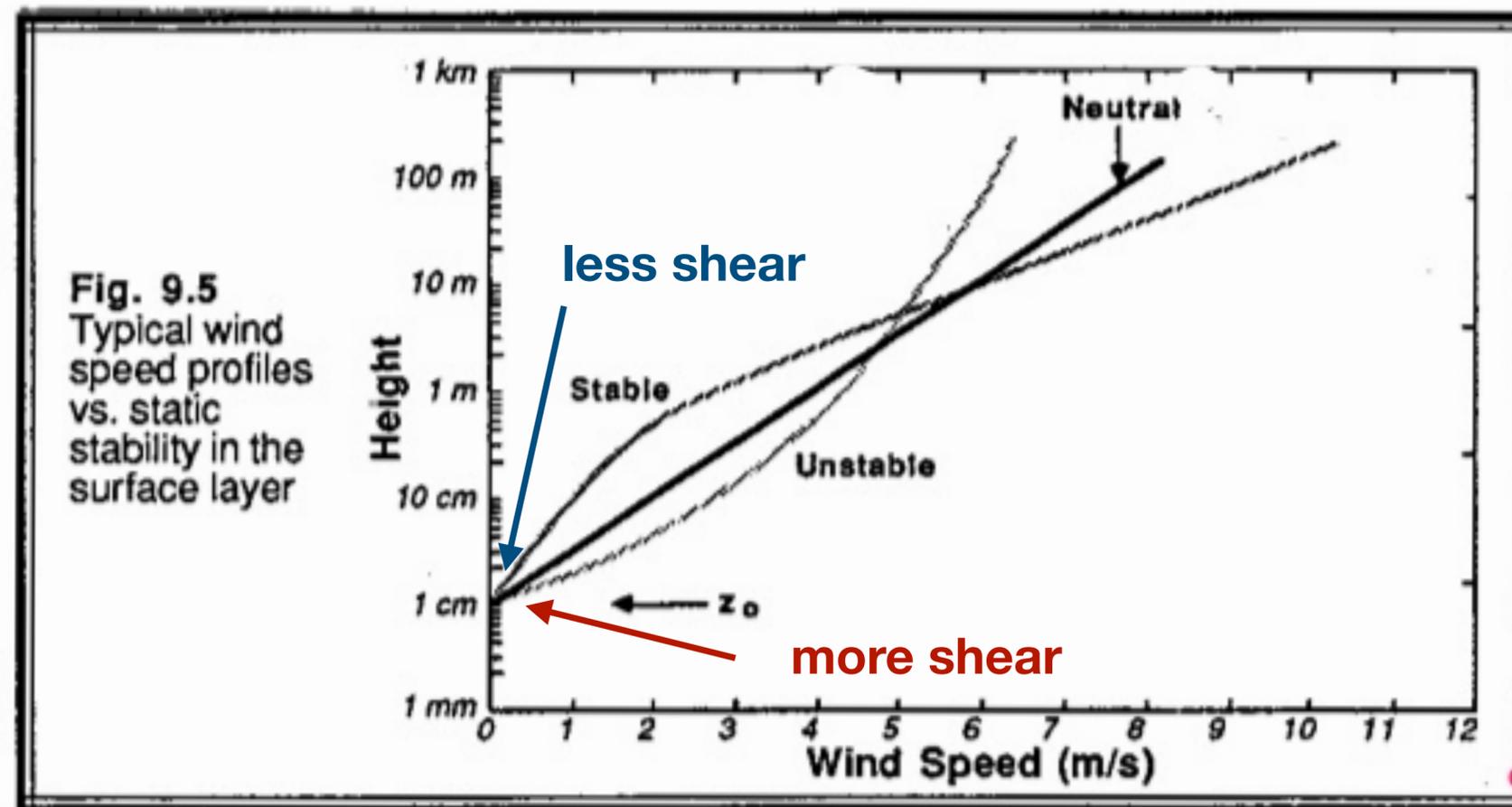
$$\frac{k}{u_*} \frac{d\bar{U}}{d \ln z} = 1$$

$$\bar{U}(z) = \frac{u_*}{k} \ln \frac{z}{z_0}$$

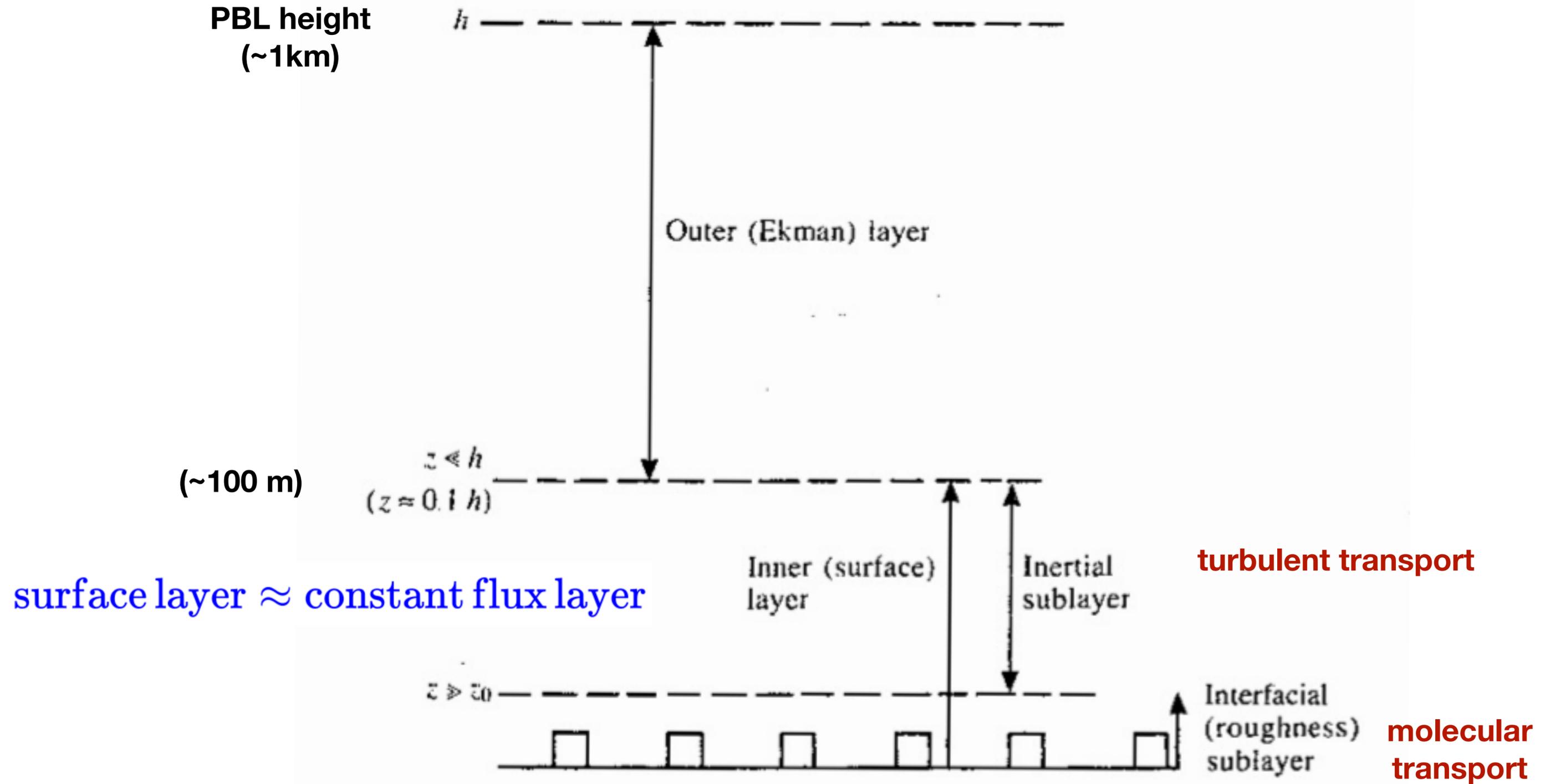
Diabatic

$$\frac{k}{u_*} \frac{d\bar{U}}{d \ln z} = \phi_m \left(\frac{z}{L} \right)$$

$$\bar{U}(z) = \frac{u_*}{k} \left(\ln \frac{z}{z_0} + \psi_m \left(\frac{z}{L} \right) \right)$$



Bulk Flux Parameterizations



Bulk Flux Parameterizations

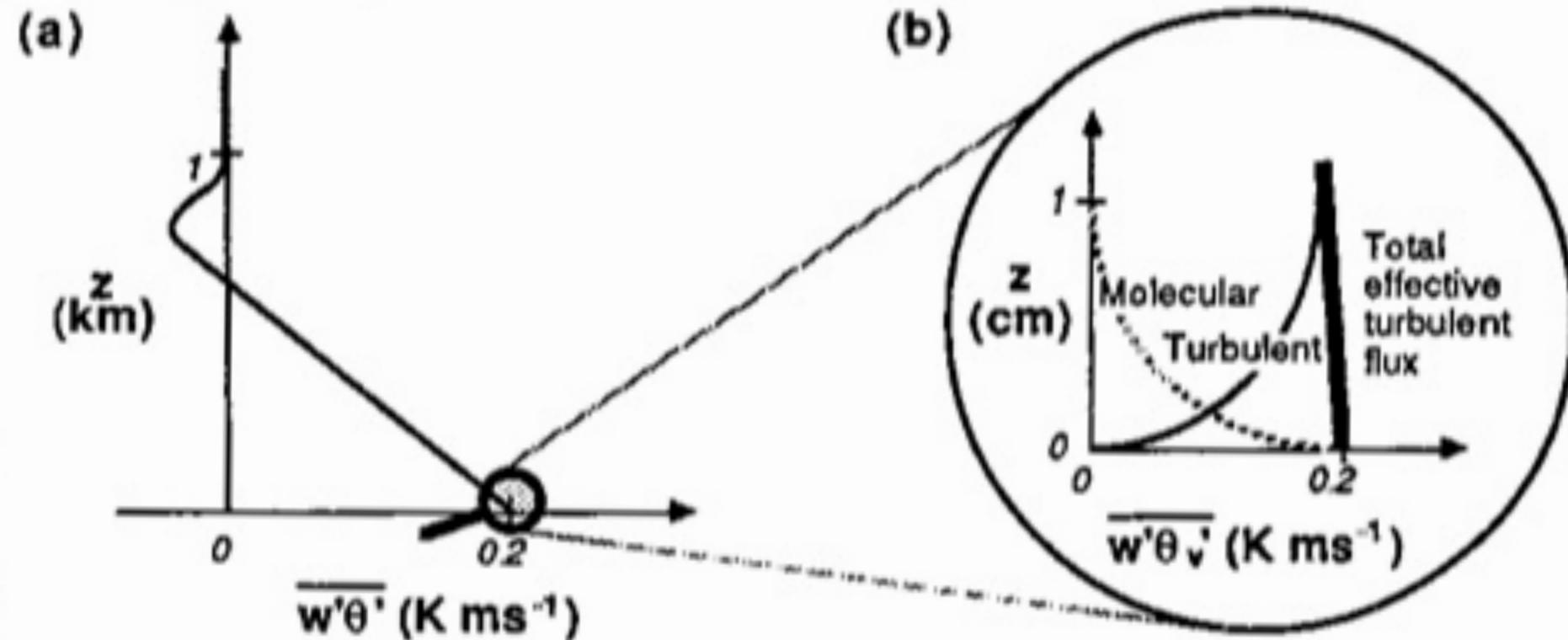
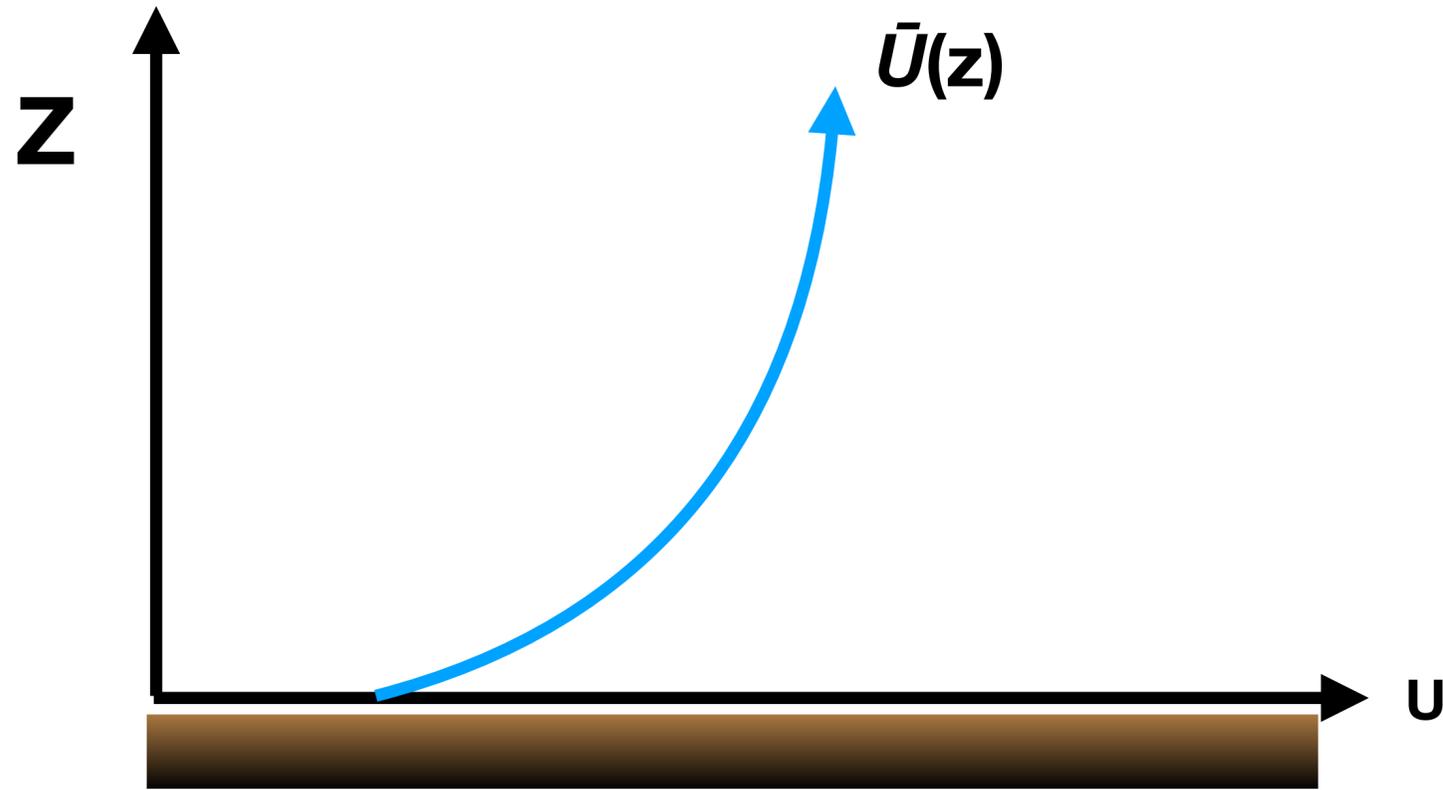


Fig. 7.1 (a) The effective turbulent heat flux using daytime convective conditions as an example, may be nonzero at the surface. (b) This effective flux, however, is the sum of the actual turbulent flux and the molecular flux.

- total flux is constant with height in surface layer
- at surface (“wall”), turbulence vanishes (no slip condition)
- away from surface (wall), molecular diffusion relatively small
- bulk methods attempt to avoid these complexities

**Bulk Fluid—away from interface
—encompasses all processes**



$\rho \bar{u}$ \equiv horizontal momentum
 $\bar{u} \cdot \rho \bar{u}$ \equiv horizontal advection of
horizontal momentum

$$\tau = C_D \cdot [\bar{u} \cdot \rho \bar{u}]$$

C_D \equiv fraction of horizontal momentum
“lost” to surface
Typically, $C_D \sim 0.001 - 0.005$

Bulk Flux Parameterizations

- τ constant with height
- C_D , \bar{u} vary with height
- select ref height, say 10 m

$$\frac{\tau}{\rho} = u_*^2 = C_{D10} U_{10}^2$$

Bulk Heat Flux Parameterization

$$\frac{H}{\rho C_p} = \overline{w'T'} = -C_{H10} \cdot \underbrace{\bar{U}_{10}}_{\text{mean horizontal advection of heat at 10 m height}} (T_{10} - T_0)$$

vertical turbulent heat flux

$$C_{H10} = \frac{\text{vertical turbulent flux}}{\text{bulk horizontal advection}}$$

- fraction of horizontal heat flux transferred to surface
- efficiency of transport to surface

Drag coefficient vs stability

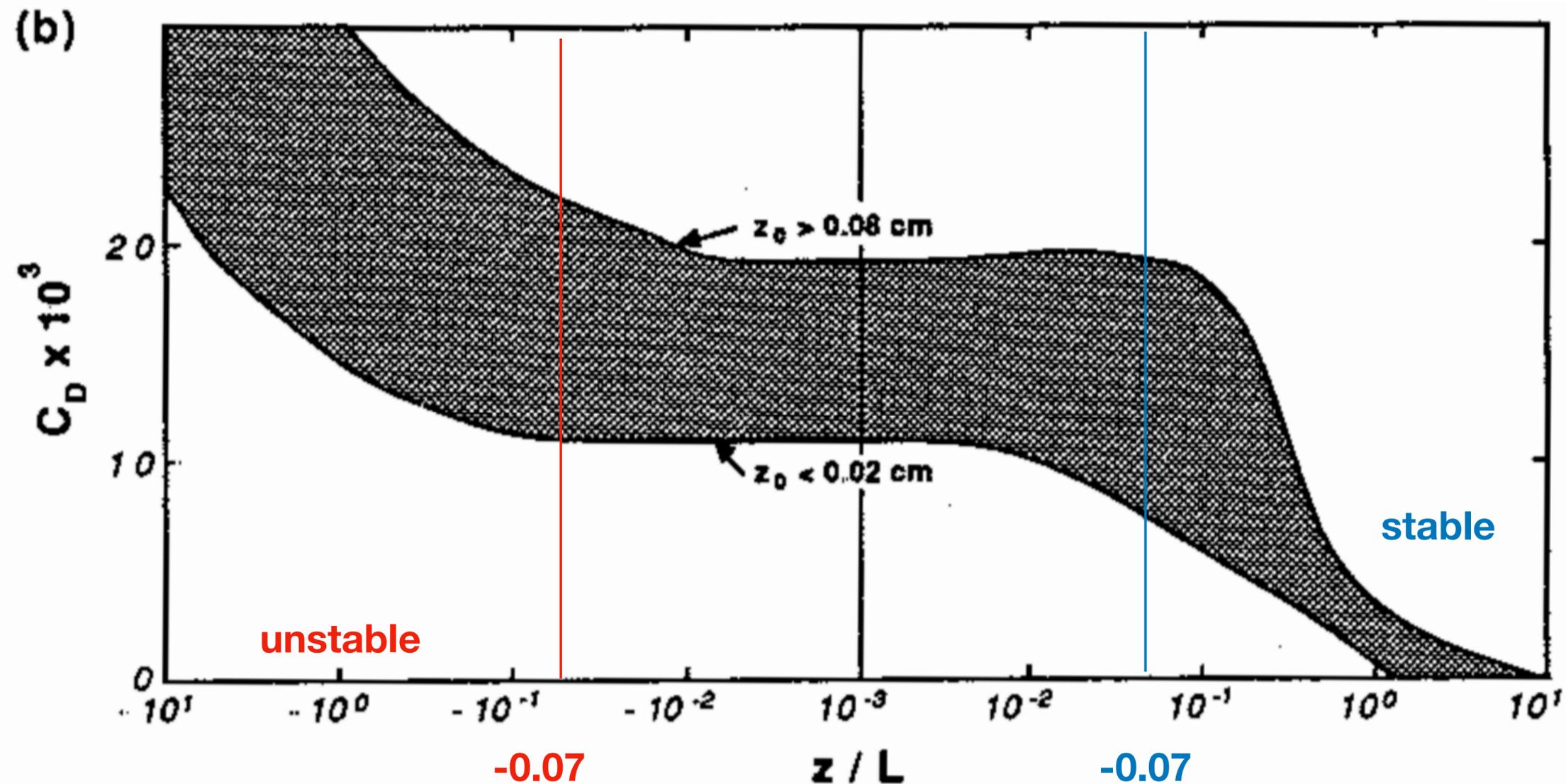
non-neutral (diabatic)

$$C_D = k^2 \left[\ln\left(\frac{z}{z_0}\right) - \Psi_m\left(\frac{z}{L}\right) \right]^{-2}$$

unstable: $\Psi_m > 0, C_D \uparrow$

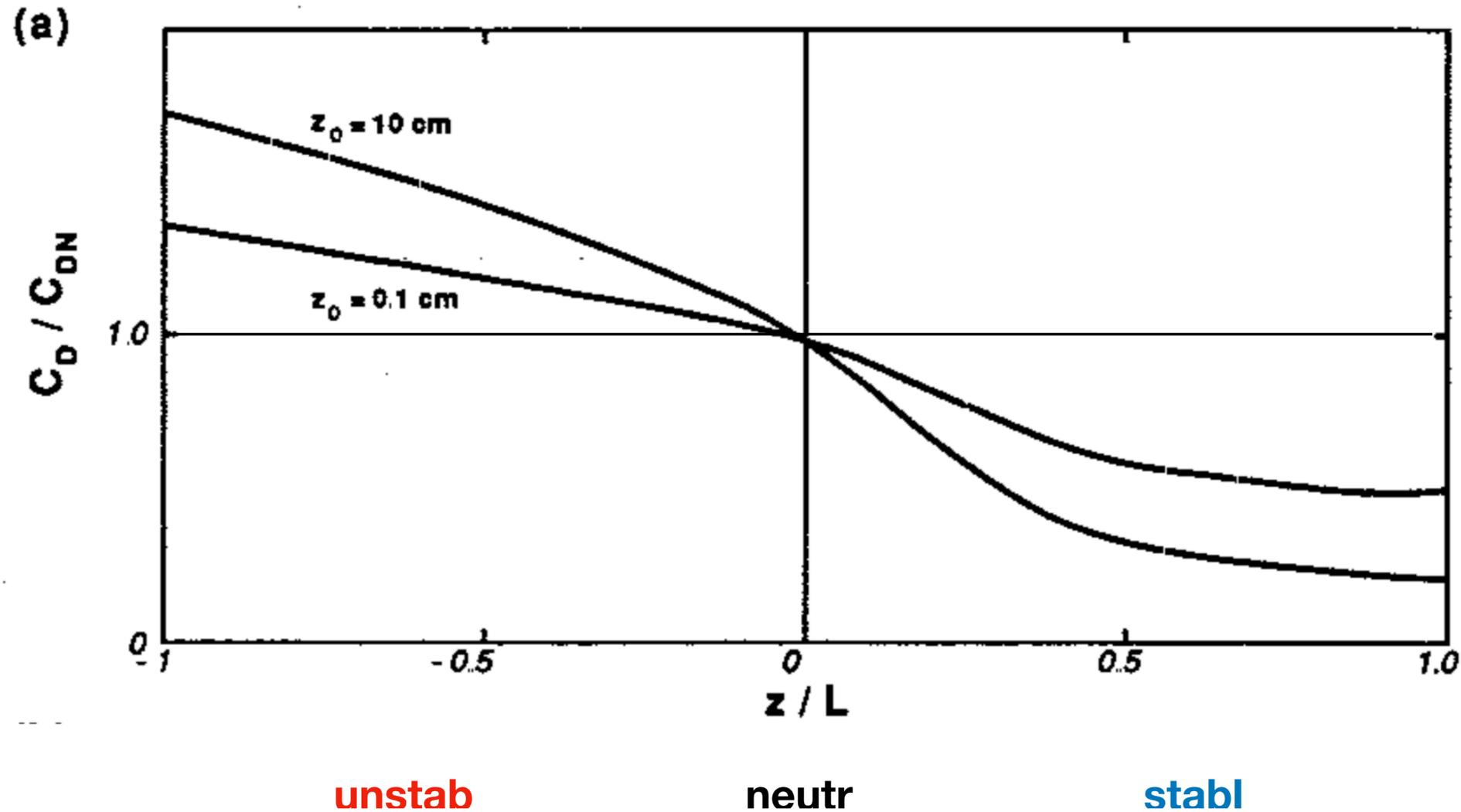
stable: $\Psi_m < 0, C_D \downarrow$

neutral: $-0.07 < z/L < 0.07$

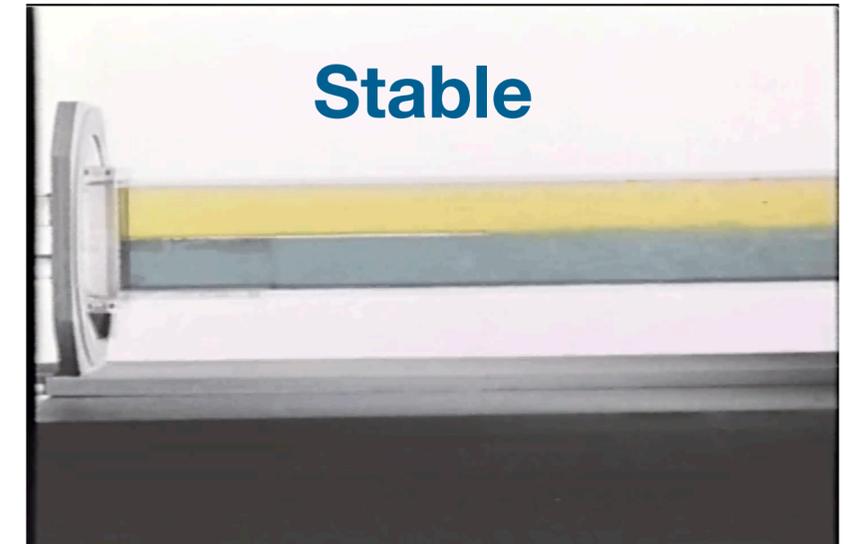


Drag Coefficient (C_D) versus Stability

$$C_{D10} = \frac{\text{vertical turbulent momentum flux}}{\text{bulk horizontal advection of momentum}}$$



Stall



~ 0.001 (efficiency 0.1%)

Bulk Flux Parameterizations

vertical flux = Coeff · [horizontal advective flux]

momentum: $\tau = C_{D10} \cdot [U_{10} \cdot \rho_a U_{10}]$

heat: $H = C_{H10} \cdot [U_{10} \cdot \rho_a c_p (\theta_s - \theta_{10})]$

moisture: $H_L = C_{E10} \cdot [U_{10} \cdot \rho_a L_v (q_s - q_{10})]$

C_D, C_H, C_E depend on $z_0, z/L, \dots$

Example drag coefficients

Table 7-3. Sample drag and bulk-transfer coefficients. After Garratt (1977), Anthes and Keyser (1979), Gadd and Keers (1970), Deardorff (1968), Verma, et al (1986), and Kondo and Yamazawa (1986a).

Coefficient	Conditions
$C_{DN} = 1.4 \times 10^{-3}$	10 m winds over plains, daytime
$C_D = 16.0 \times 10^{-3}$	10 m winds over deciduous forest
$C_D = 40.0 \text{ to } 160.0 \times 10^{-3}$	10 m winds over coniferous forest
$C_{DN} = [0.75 + 0.067 \cdot M] \times 10^{-3}$	10 m winds over water

Roughly 0.1% to 4% of horizontal momentum advecting over surface
is transferred down to the surface

Drag and Roughness, z_0

$$\frac{\tau}{\rho} = u_*^2 = C_D U^2$$
$$C_D = \frac{u_*^2}{U^2}$$

Intuitively, the more rough the surface \implies more drag

Recall, for neutral conditions: $\bar{U}(z) = \frac{u_*}{k} \ln \frac{z}{z_0}$ ($\uparrow z_0, \downarrow U$)

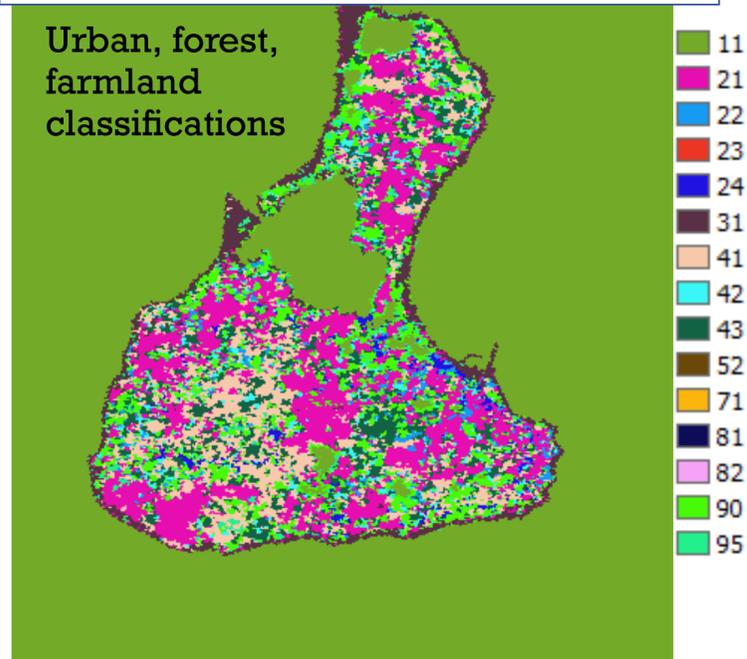
Rewrite as $\frac{u_*}{U(z)} = k \left[\ln \frac{z}{z_0} \right]^{-1}$

$$C_D = \frac{u_*^2}{U(z)^2} = k^2 \left[\ln \frac{z}{z_0} \right]^{-2} \quad (\uparrow z_0, \uparrow C_D)$$

Surface Roughness

Getting it right crucial to accurate wind resource assessment
While working on the Deepwater Offshore Wind Project off of Block Island, RI....

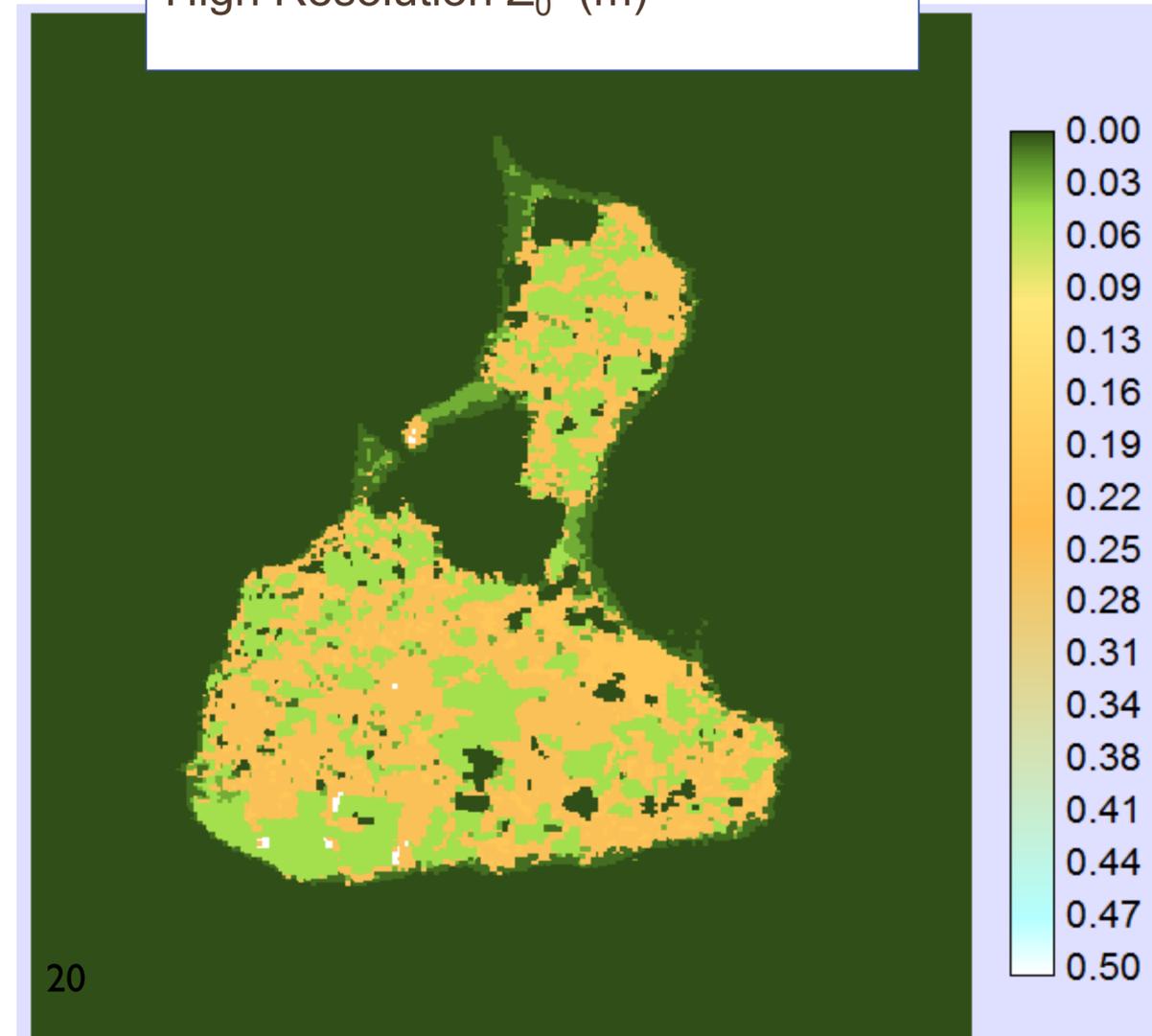
Existing: NLCD/Landsat



Site Photography



High Resolution Z_0 (m)

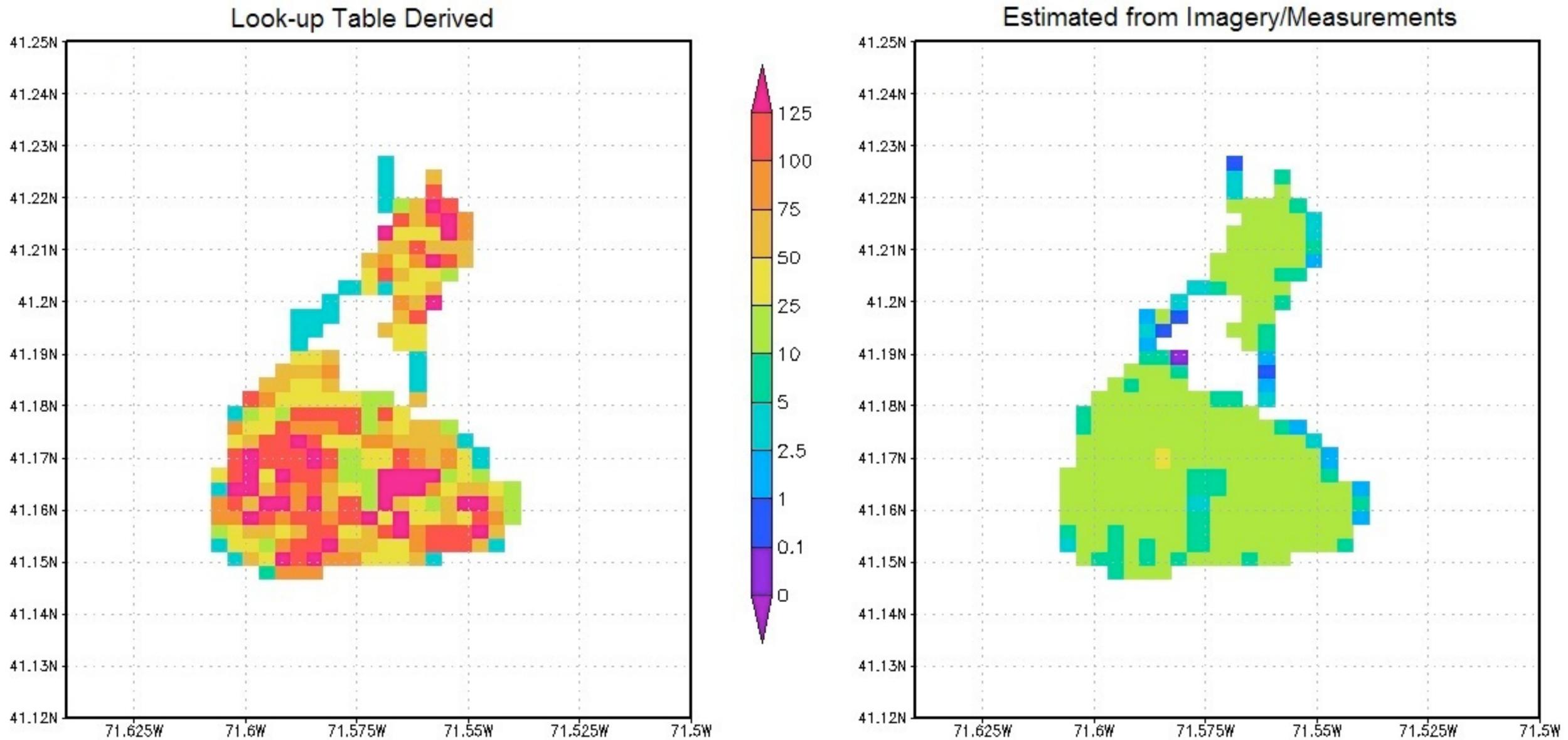


Aerial Photography



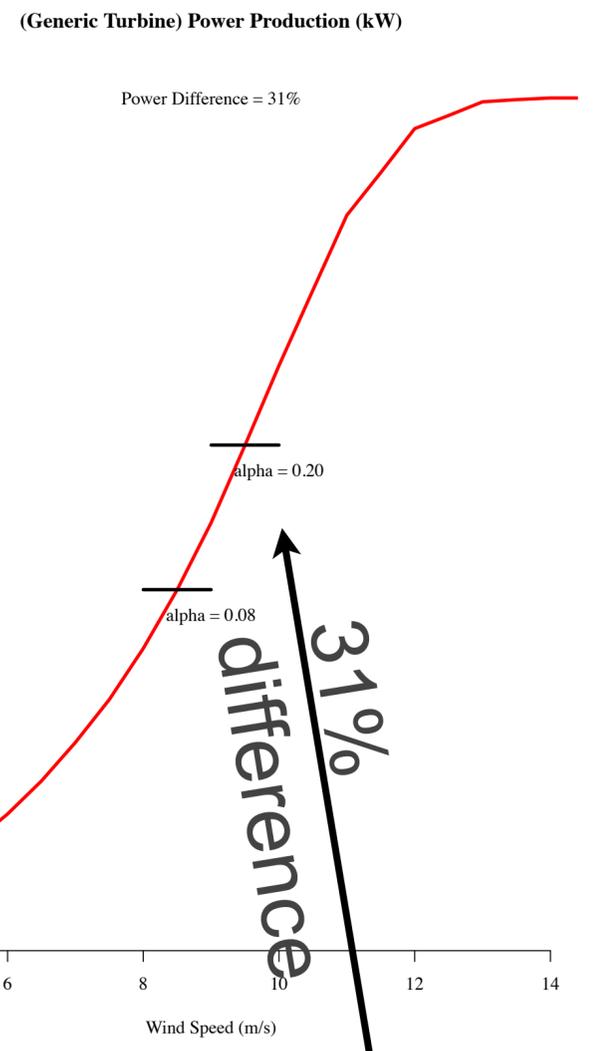
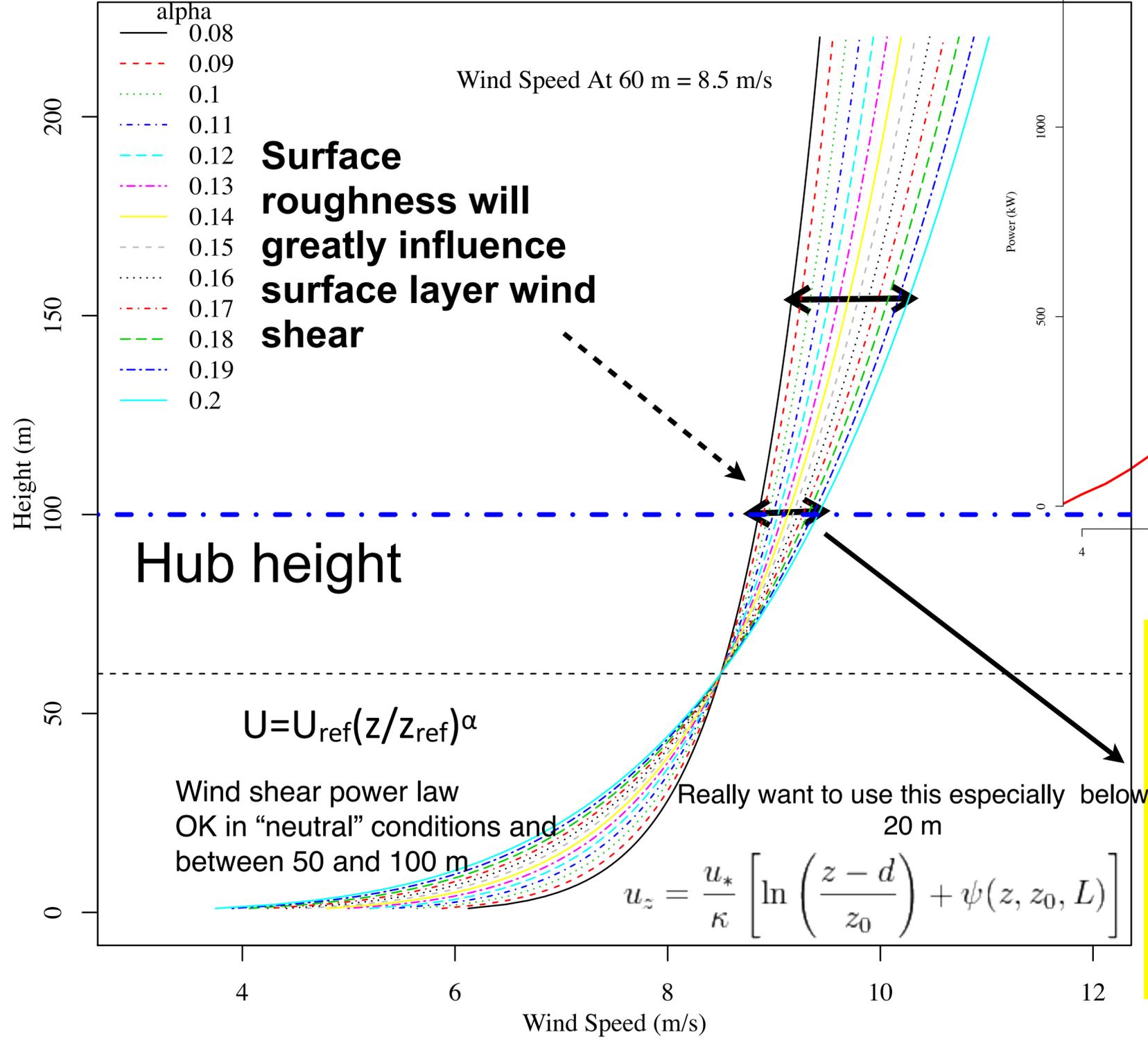
Comparison of Model Roughness Fields—from WRF

Block Island – Roughness (cm)



~1 m difference in model roughness fields – Variability within land cover classes

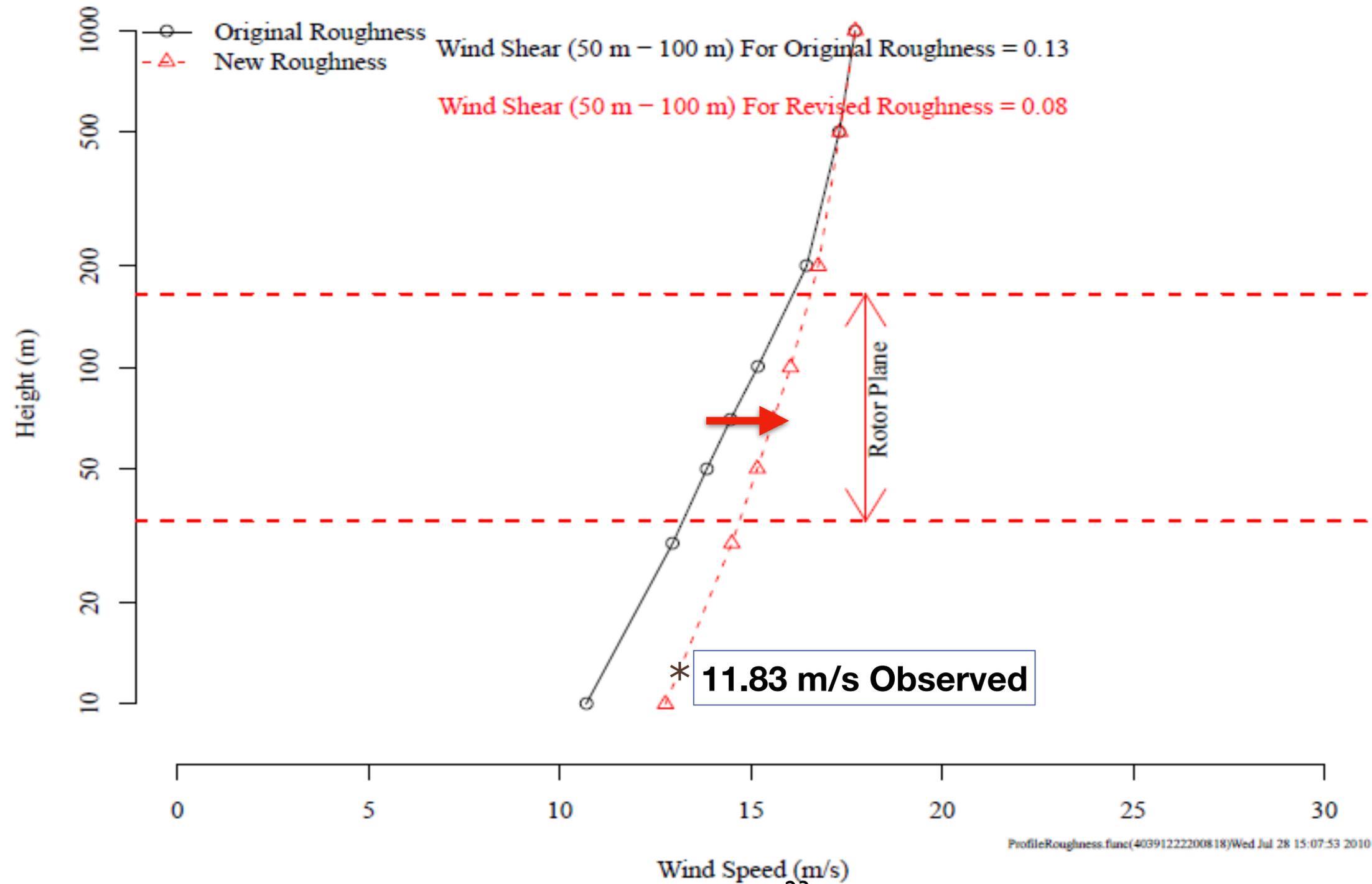
Wind Speed Sensitivity To Shear Exponent (at Hm = 60 m)



This can certainly affect power production estimates as surface roughness has great influence over the wind profile (shear) in the lowest 100s of meters

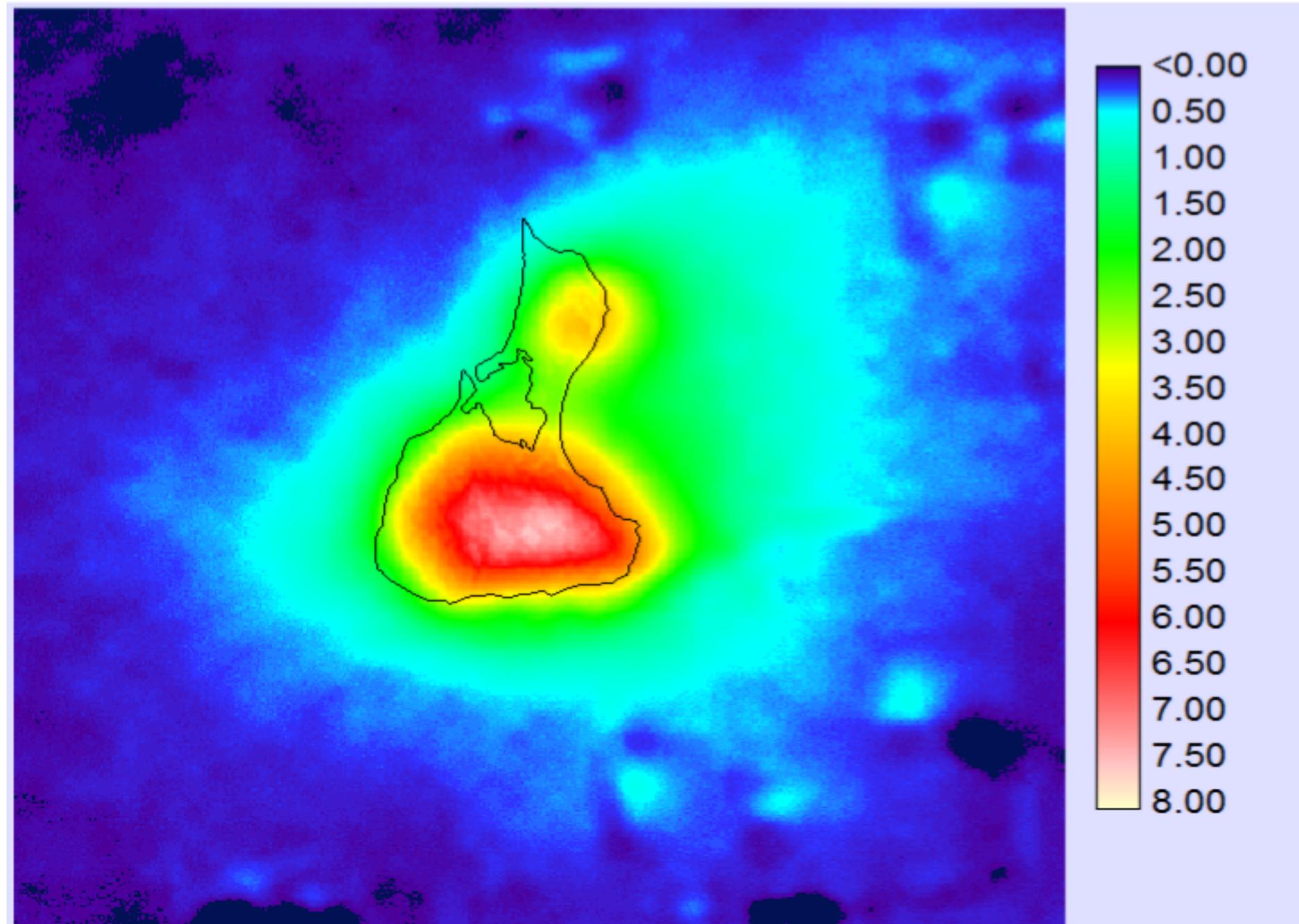
Results – Wind Speed Profile (KBLI)

MASS 1 km Wind Profile At -71.58 41.17 (Points 40,39) Date = 12/22/2008 Hour = 1800 GMT



Energy Production Estimates

Use of new roughness map increased capacity factor over 8% in southern sections of Block Island



Surface Energy Balance

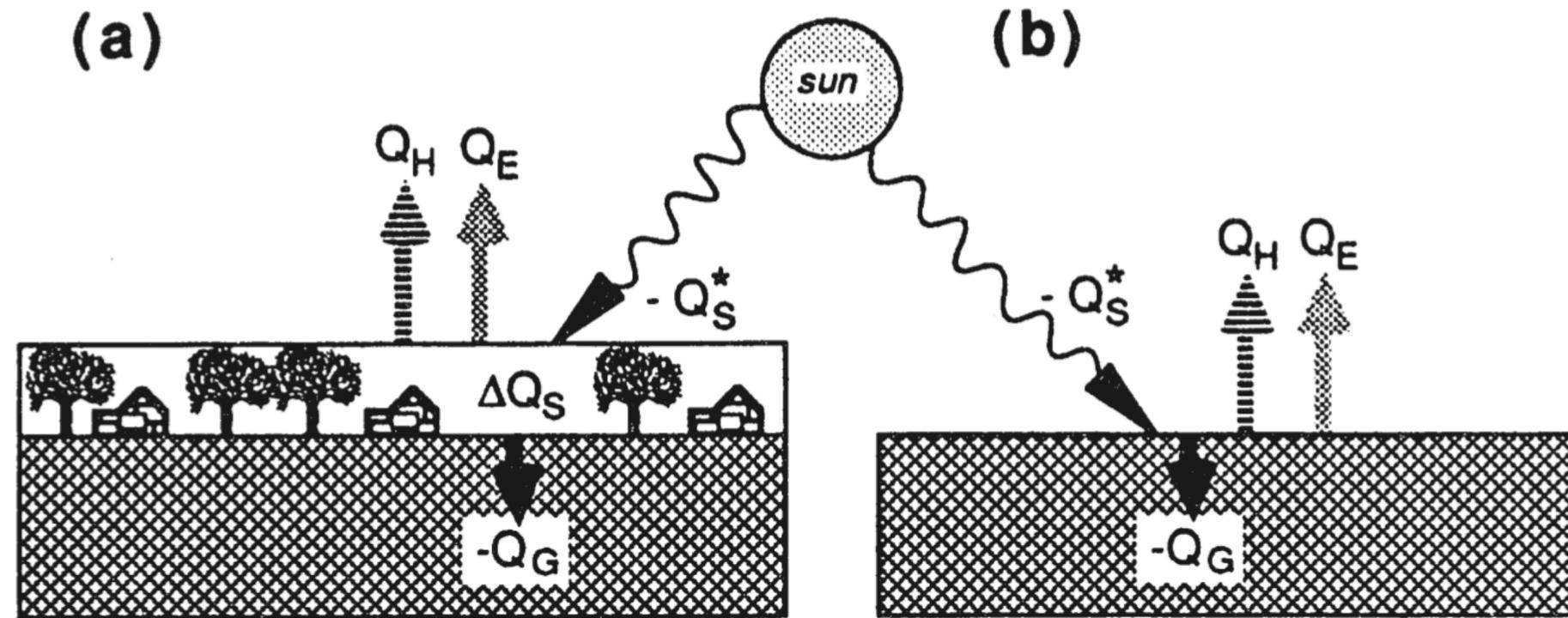


Fig. 7.2 Contributions to the surface energy balance (a) for a finite thickness box and (b) for an infinitesimally thin layer. $-Q_s^*$ is the net radiative contribution, Q_H is turbulent sensible heat flux, Q_E is turbulent latent heat flux, $-Q_G$ is molecular flux into the ground, and ΔQ_s is storage.
Stull 1988

$$-Q_s^* = Q_H + Q_E - Q_G + \Delta Q_s \quad (7.2b)$$

- Q_s^* = net upward radiation at the surface
- Q_H = represents the upward sensible heat flux out of the top
- Q_E = represents the upward latent heat flux out of the top
- Q_G = represents the upward molecular heat flux into the bottom
- ΔQ_s = denotes the storage or intake of internal energy (positive for warming and for chemical storage by photosynthesis).

Surface energy balance

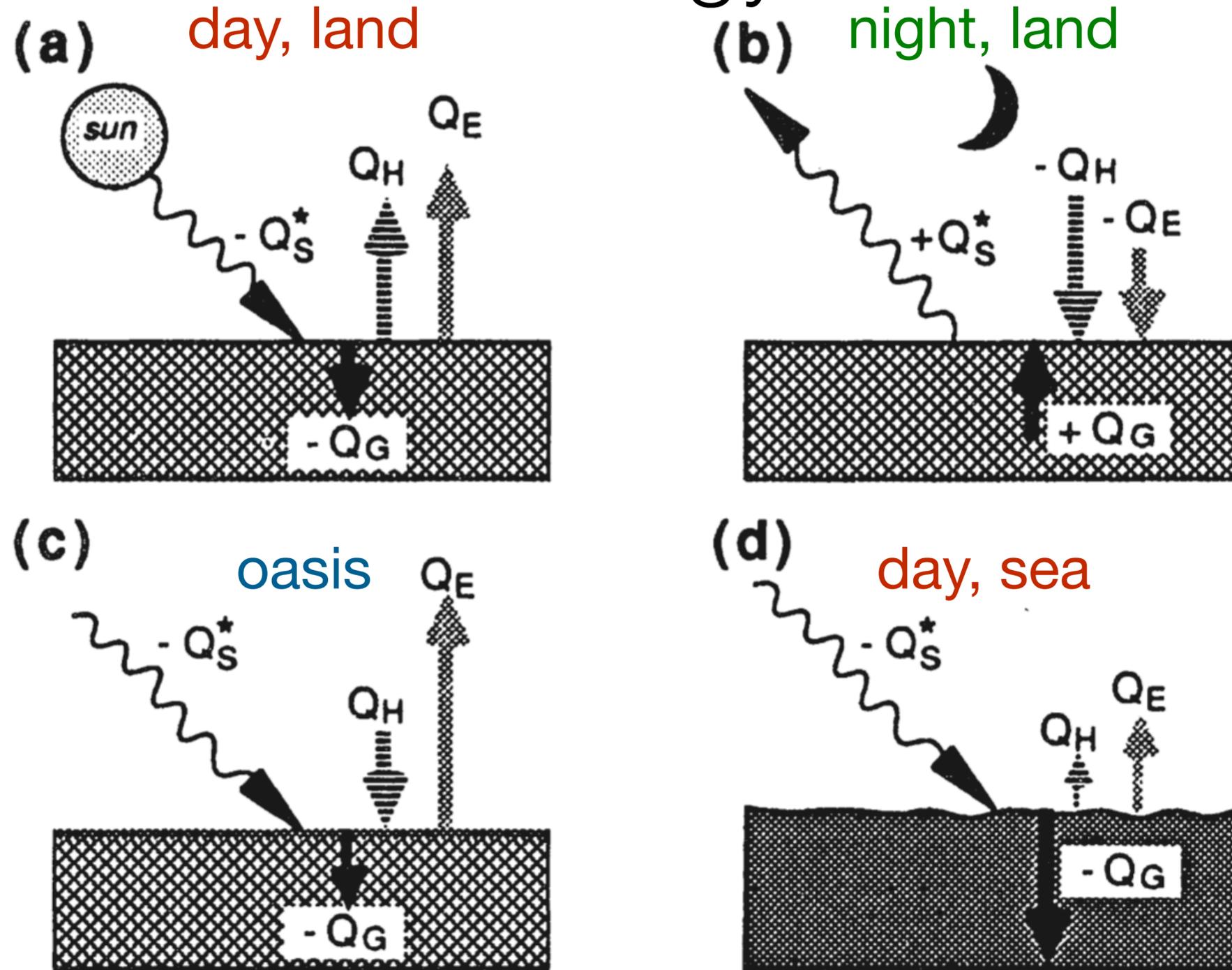
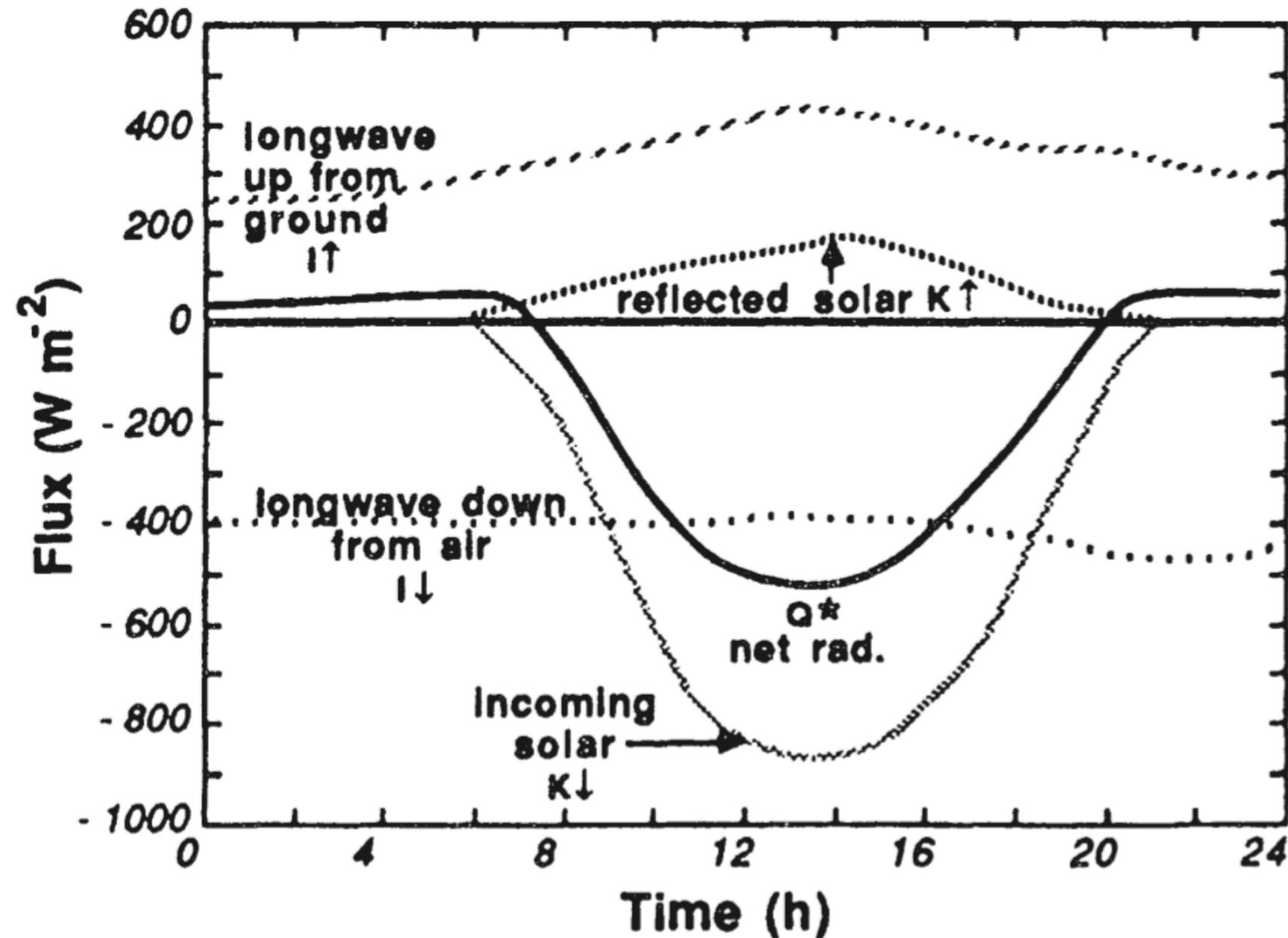


Fig. 7.3 Typical variation of terms of the surface energy balance for (a) daytime over land; (b) nighttime over land; (c) oasis effect of warm dry air advection over a moist surface; and (d) daytime over the sea with no advection. Arrow size indicates relative magnitude.

Stull 1988

Surface Energy Balance—Radiation Components

Fig. 7.5 Stull 1988
Surface radiation budget components for 30 July 1971, at Matador, Saskatchewan (50°N) over a 0.2 m stand of native grass. Cloudless skies in the morning, increasing clouds in the late afternoon and evening (after Ripley and Redmann, 1976).

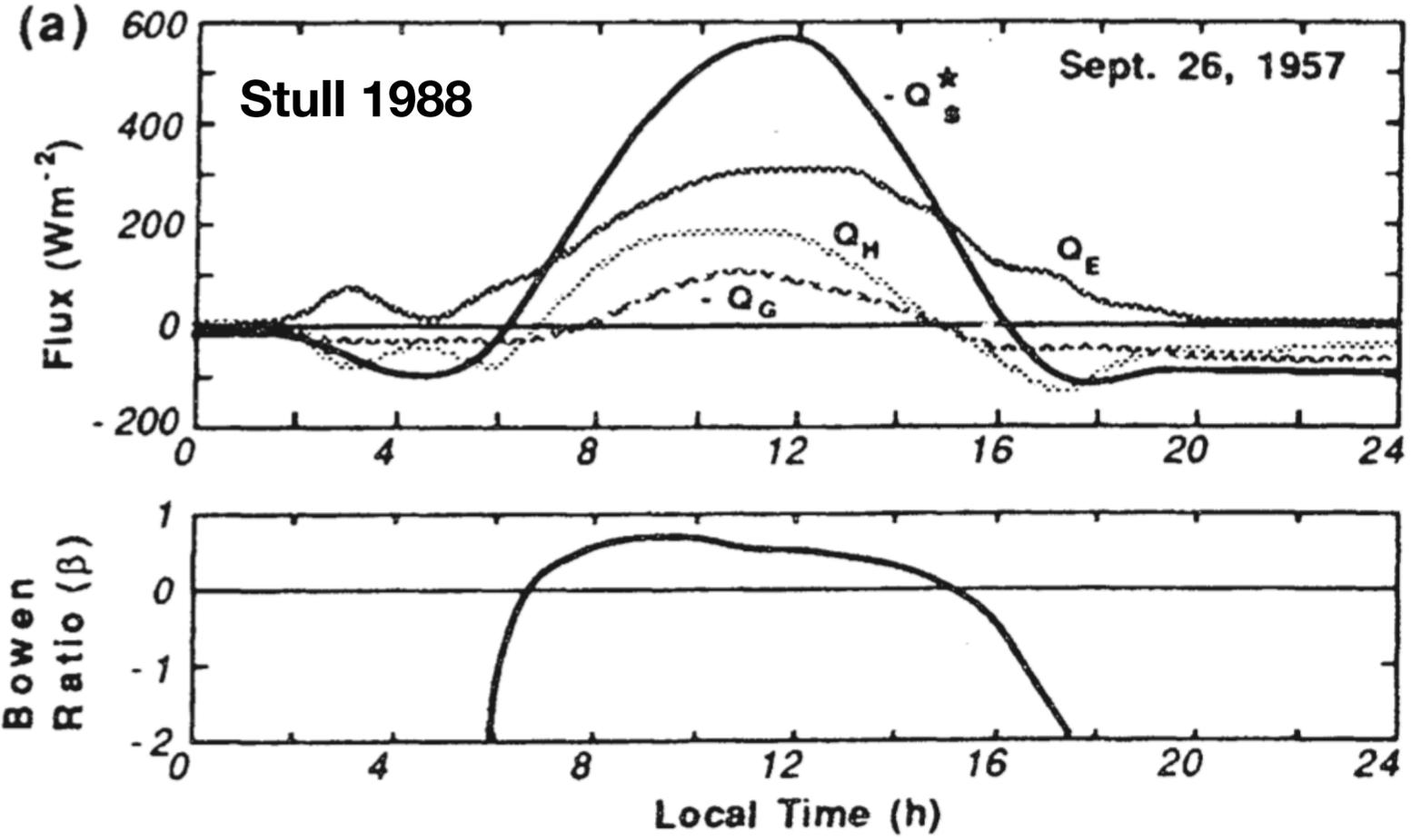


126 NYSM standard sites measure incoming solar
18 NYSM flux sites measure all 4 components (radiation)

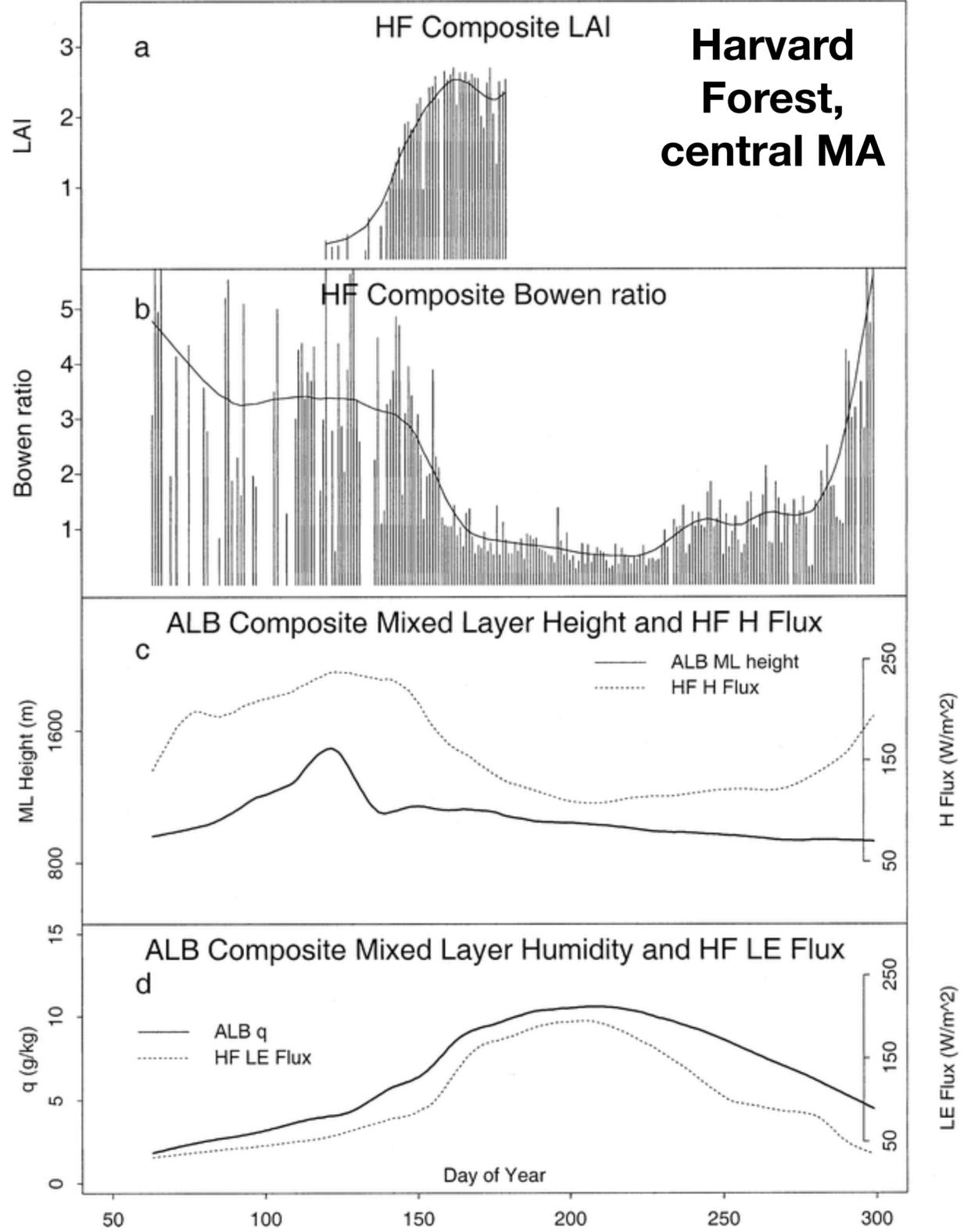
Surface Energy Balance—Fluxes, Bowen Ratio

$$\beta = \frac{Q_H}{Q_E} = \frac{\text{sensible heat}}{\text{latent heat}}$$

irrigated crop field



$\beta < 1$ for moist surface $\beta > 1$ for dry surface



Surface Energy Balance—NYSM Leafout

$$\beta = \frac{Q_H}{Q_E} = \frac{\text{sensible heat}}{\text{latent heat}}$$

- Standard Sites (126)
- ▲ Profiler Sites (17)
- Flux Sites (17)
- ✱ SWE Sites (20)

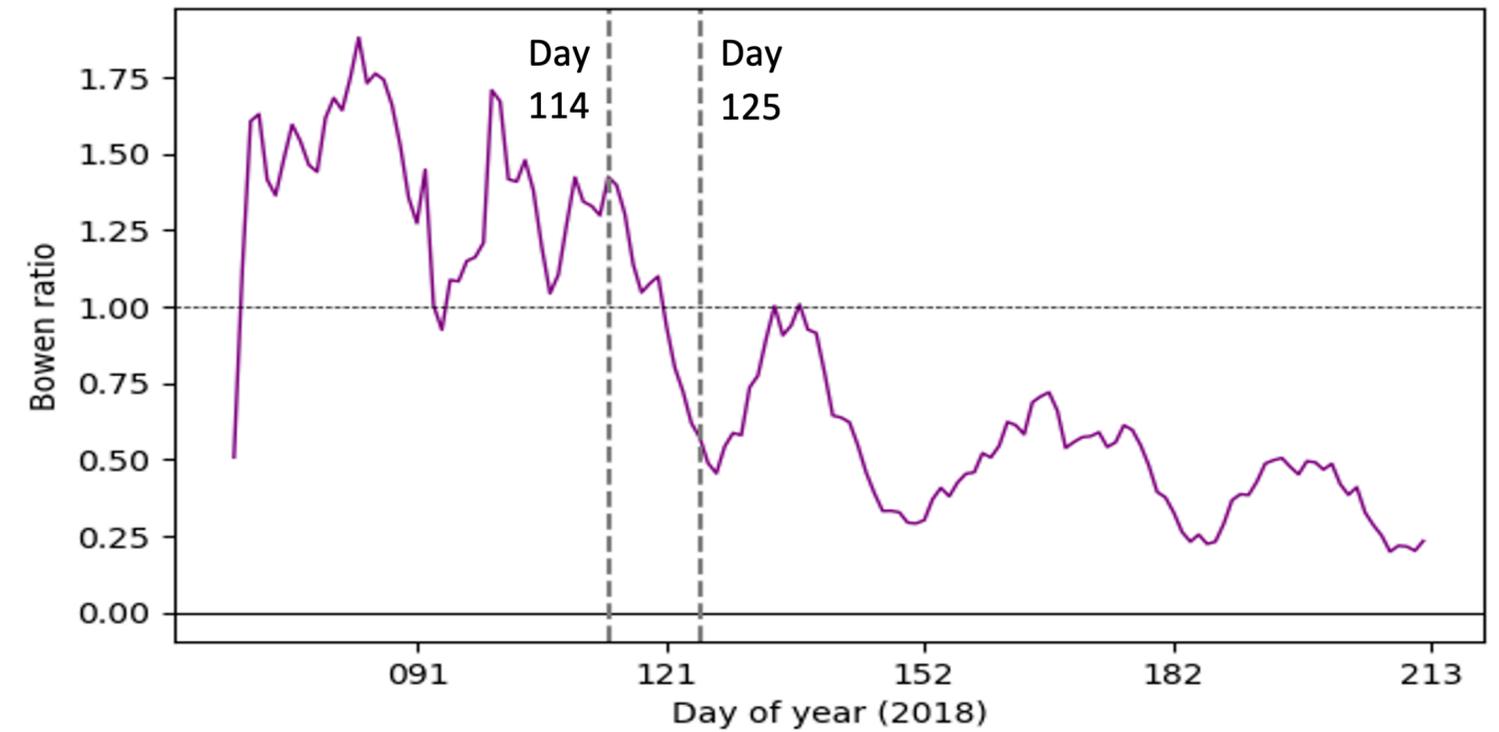
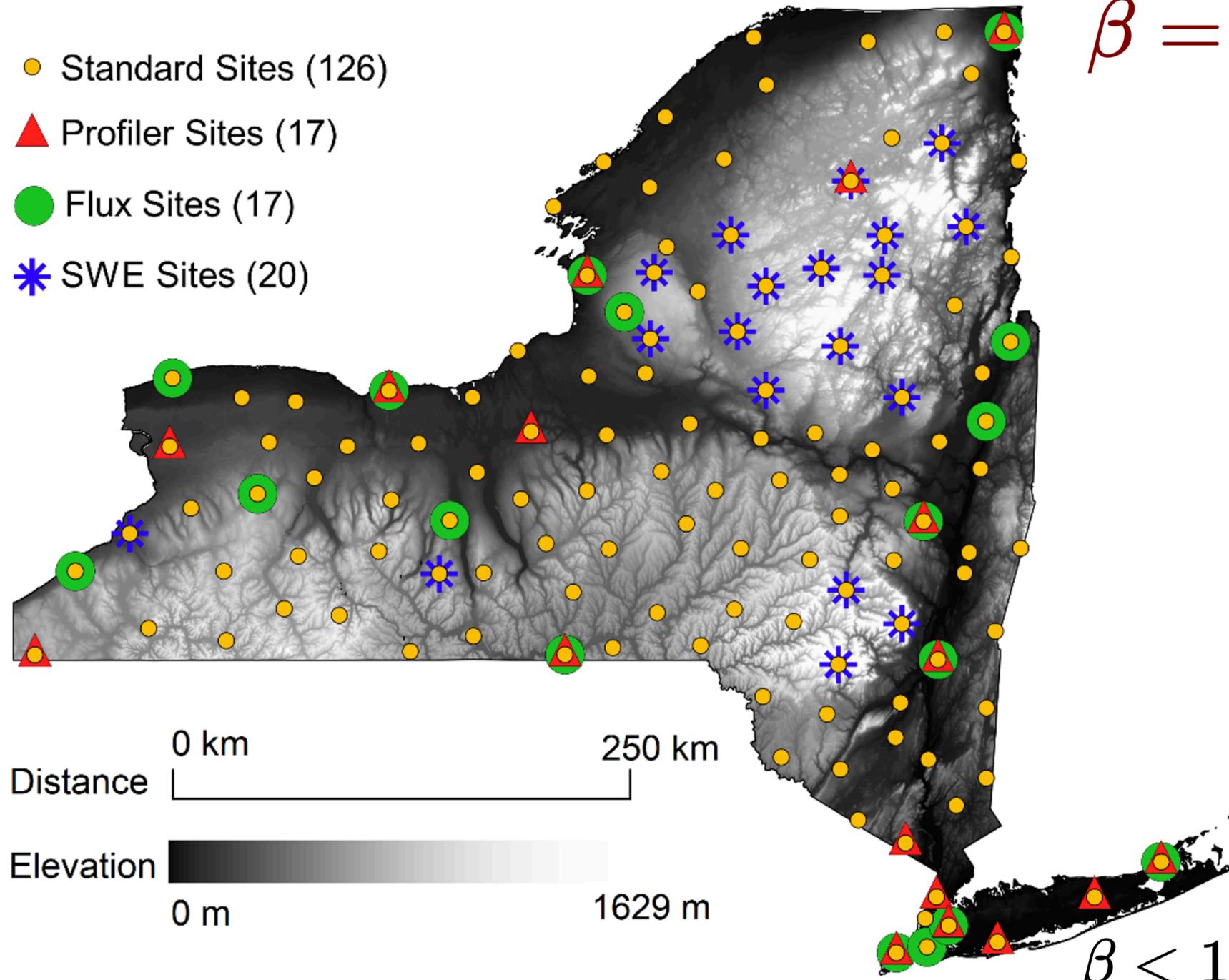


Figure 8. New York State Mesonet Flux Network average noontime (11–13 hrs) Bowen Ratio for all flux sites excluding New York City sites (BKLN, QUEE, STAT). The first vertical dotted line to the left indicates the state-wide average day of first visible grass growth (114), and the second vertical line represents the average day of first visible leaf emergence (125). Data with quality control grades 1-3 between Mar 10-Aug 1 2018 were used. Running mean ...

$\beta < 1$ for moist surface $\beta > 1$ for dry surface

Observing the ABL: vertical structure

remote: lidar, microwave radiometer



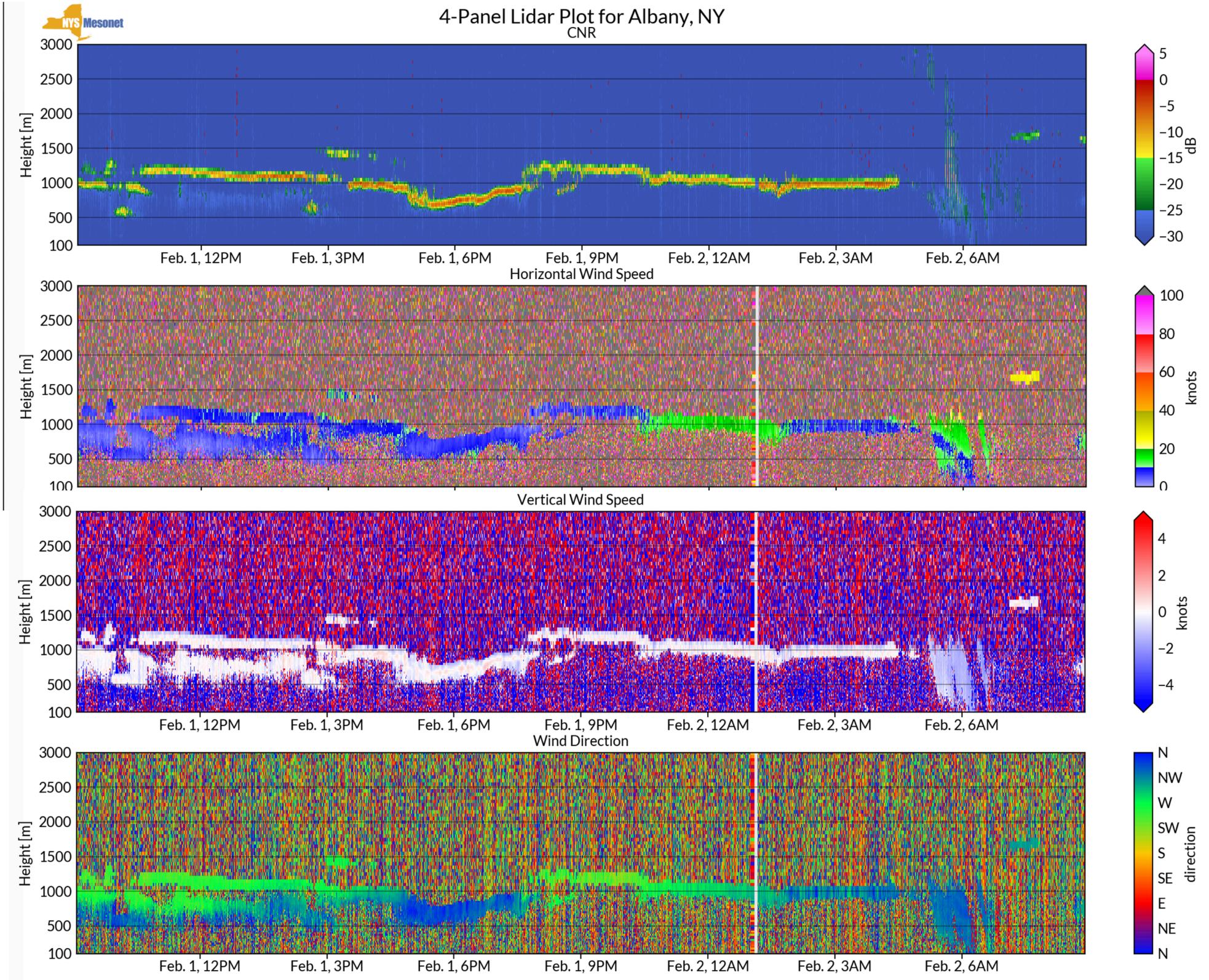
vertical wind profiles to ~3-5 km



temperature/moisture profiles to ~10 km

Feb 1-2 2020

4-Panel Lidar Plot for Albany, NY CNR



Diurnal Profile evolution

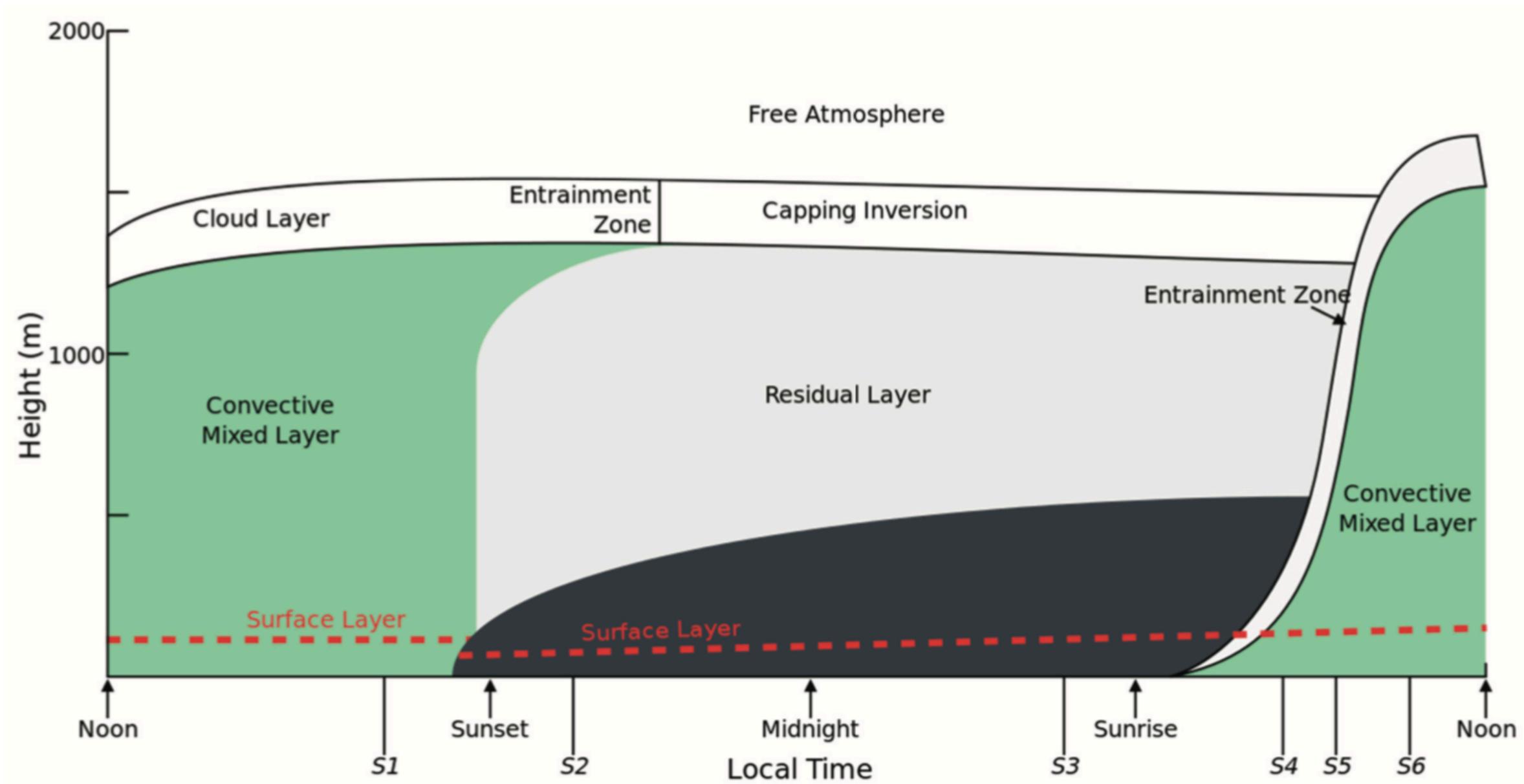


FIGURE 1. Schematic of the structure of the atmospheric boundary layer in high pressure regions over land, showing daily variations. SOURCE: Wikimedia Commons.

Boundary Layer Evolution

JOURNAL OF HYDROMETEOROLOGY

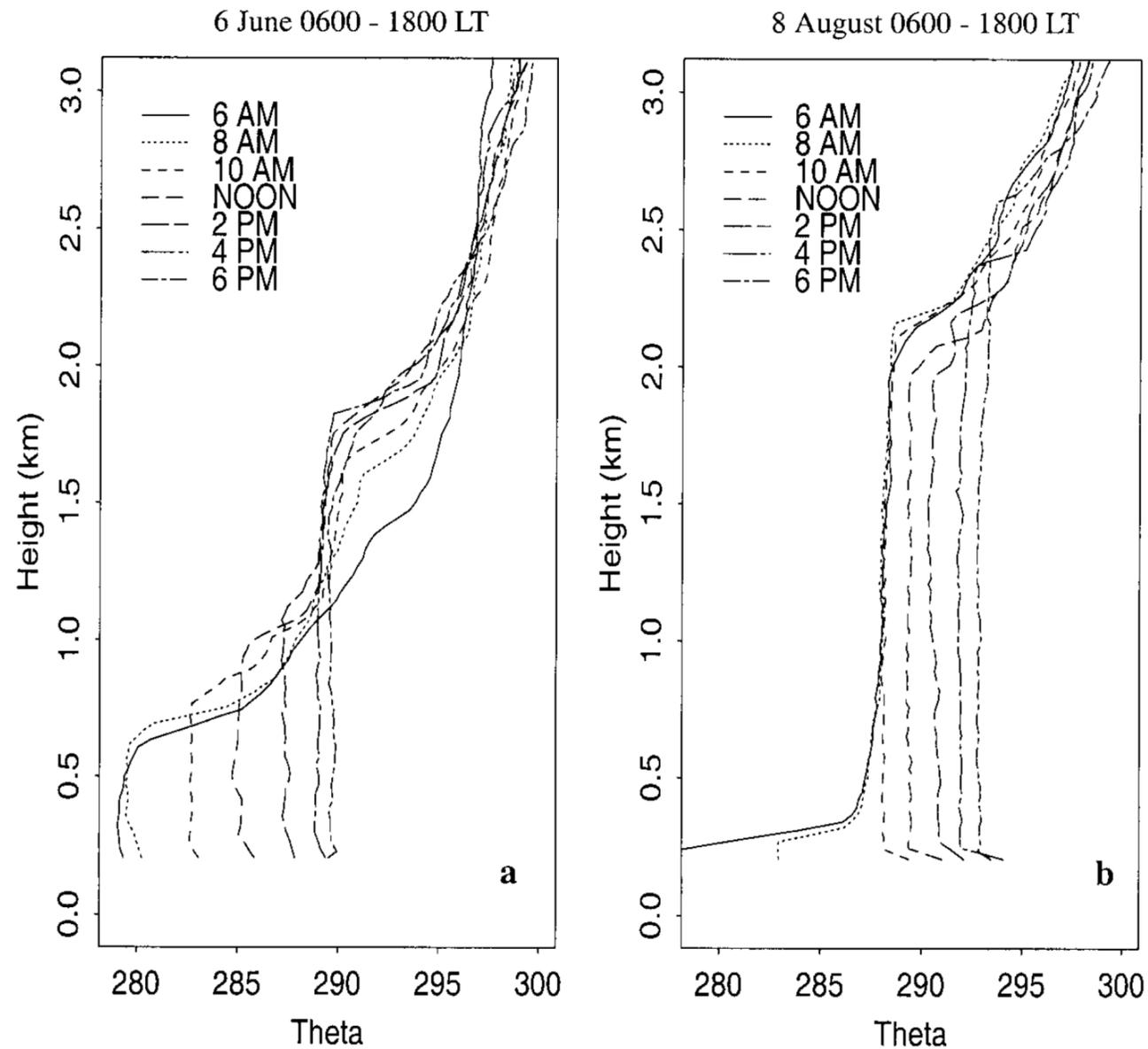


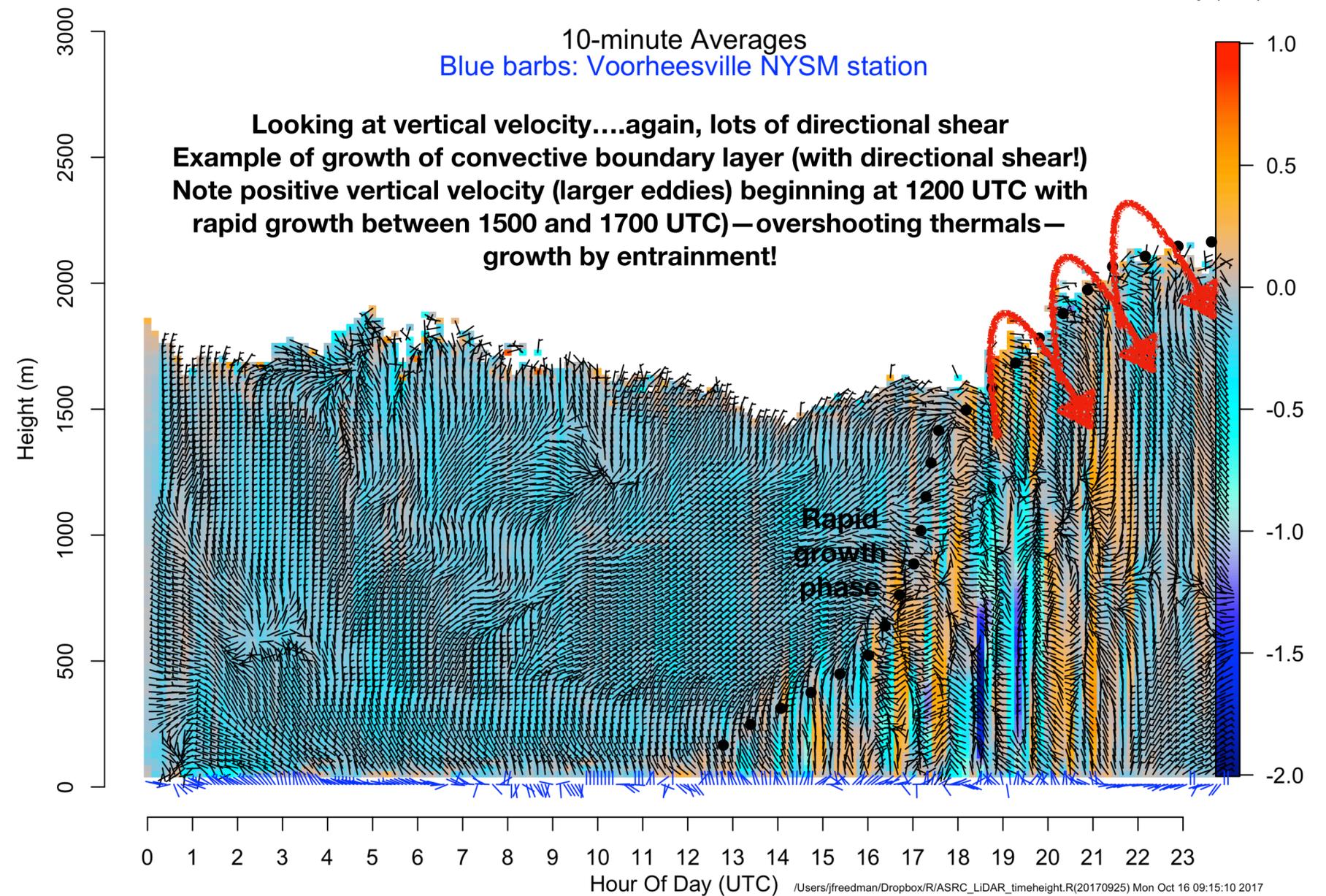
FIG. 4. BOREAS soundings from Thompson, MB, Canada, for (a) 6 Jun 1994, first day after a frontal passage, and (b) 8 Aug 1994, second day after a frontal passage.

Freedman and Fitzjarrald 2001

LiDAR Wind and Vertical Velocity Time-height Cross Section at ASRC Roof, 09/25/2017

One Full Wind Barb = 6 - 10 m/s

Filled Contours: Vertical Velocity (m/s)

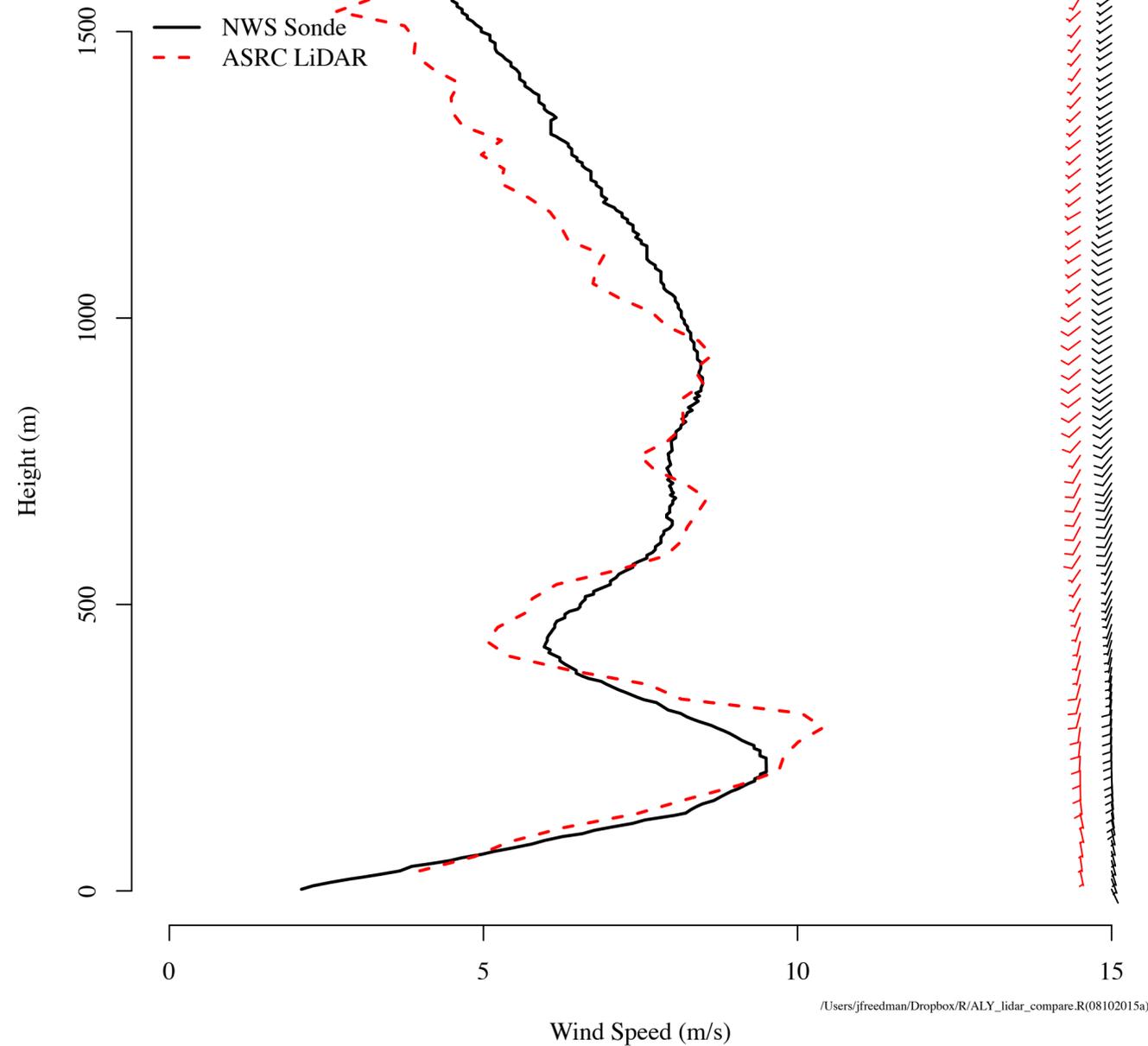


/Users/jfreedman/Dropbox/R/ASRC_LiDAR_timeheight.R(20170925) Mon Oct 16 09:15:10 2017

Early morning channelled LLJ

NWS ALY High Resolution Sounding and LiDAR Wind Profile

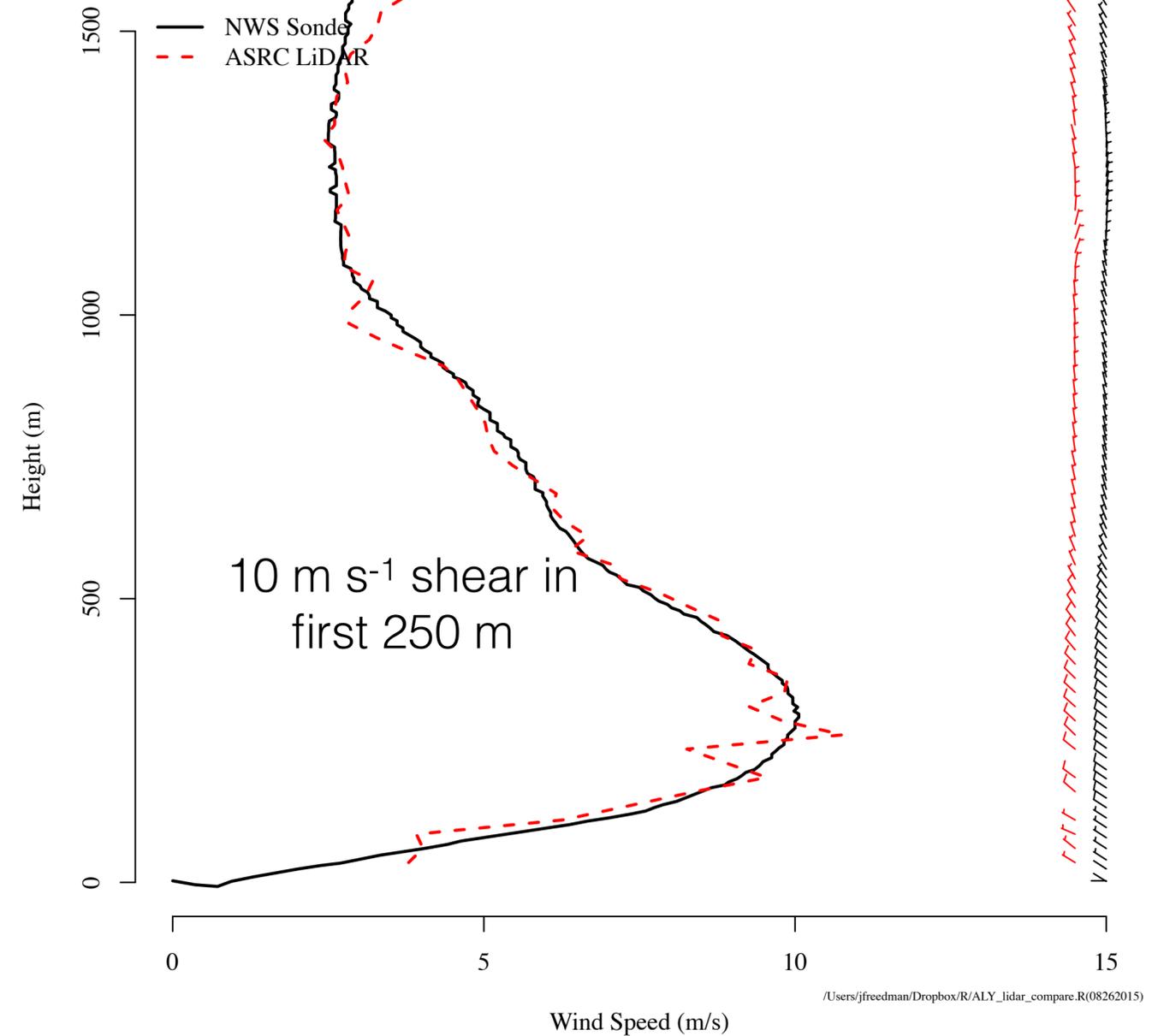
Date = 10 Aug 2015; Time: From 11:03 To 11:07



Southerly—Hudson Valley

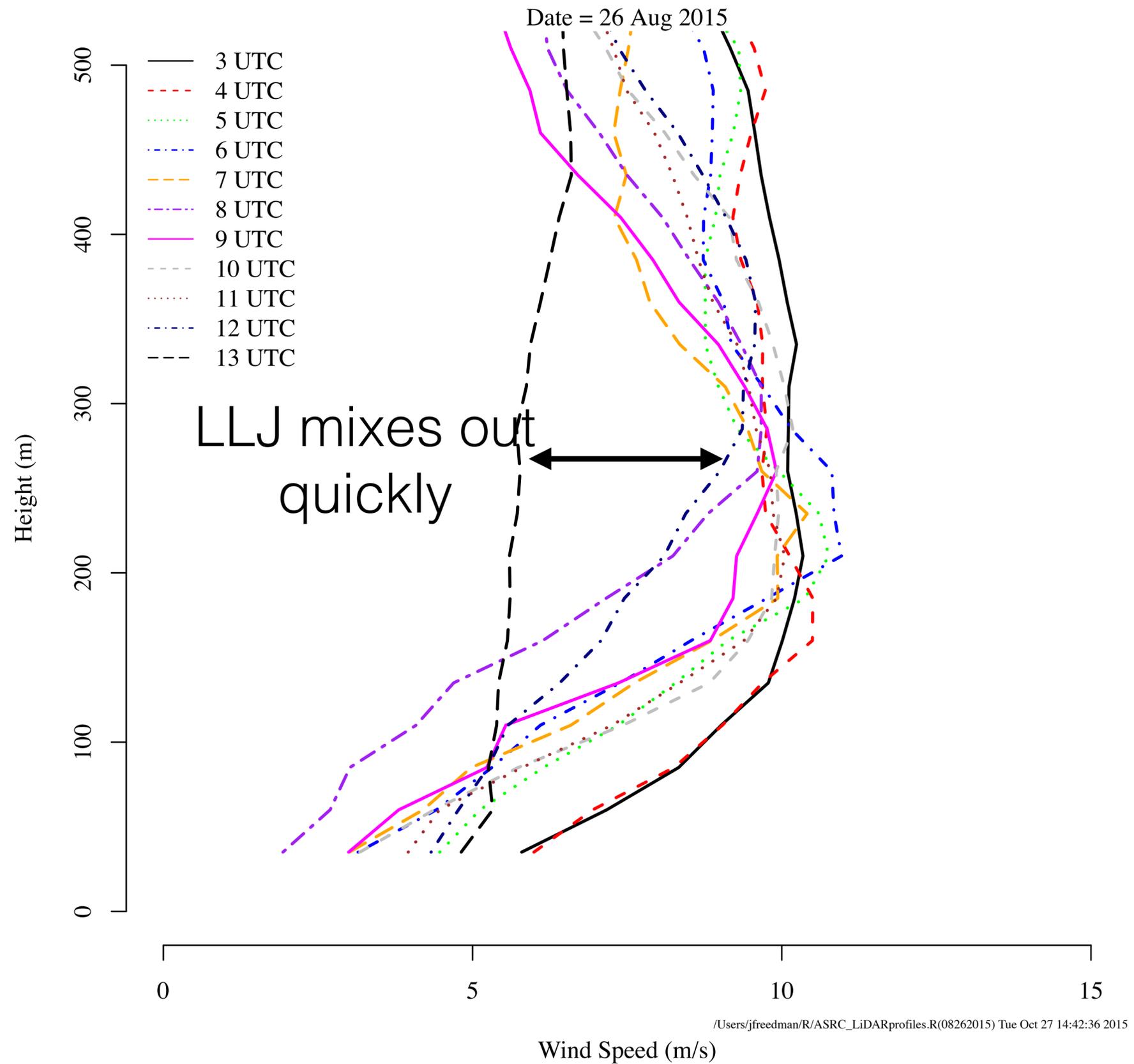
NWS ALY High Resolution Sounding and LiDAR Wind Profile

Date = 26 Aug 2015; Time: From 11:02 To 11:07



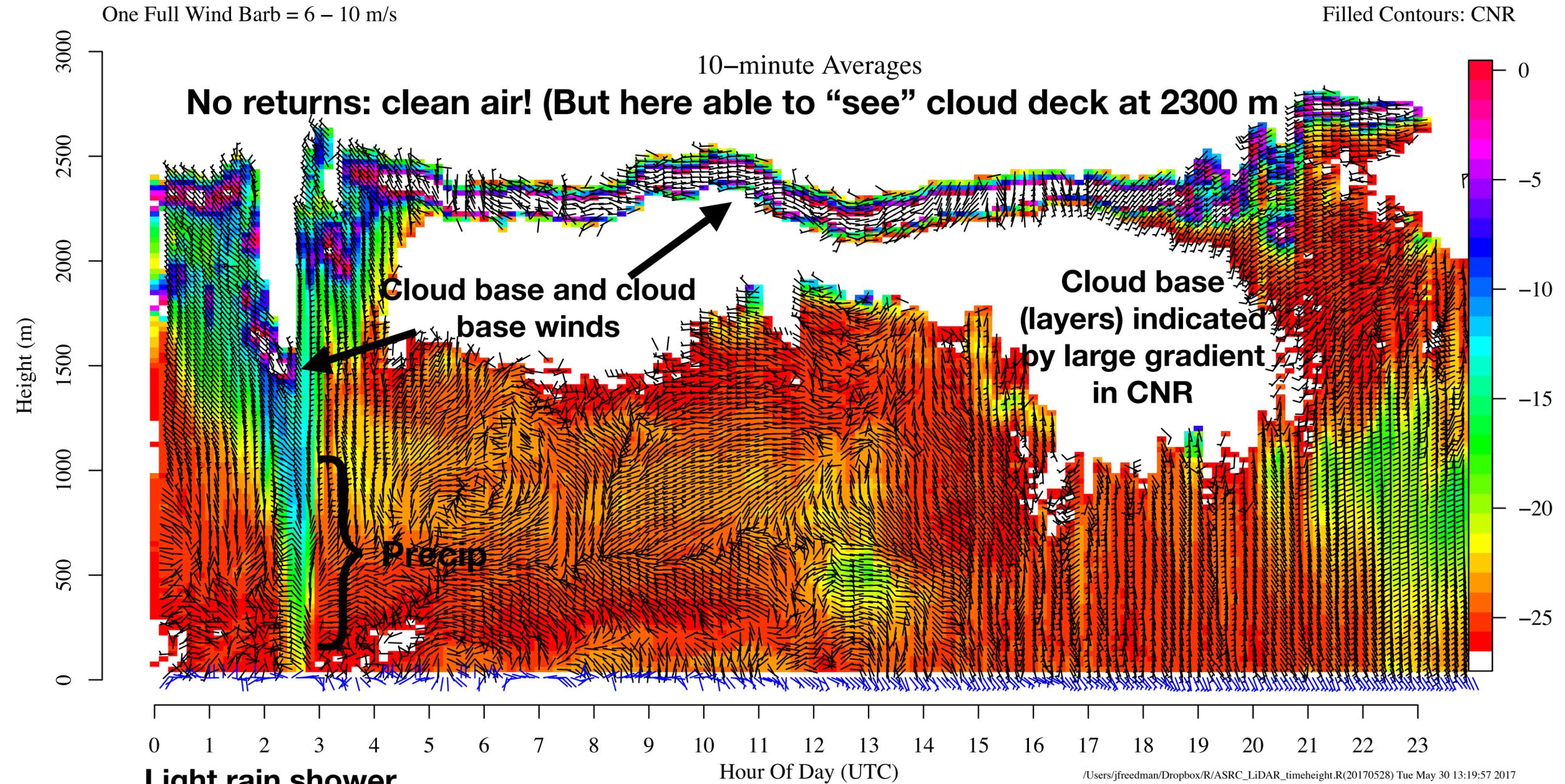
WNW—Mohawk Valley

LiDAR Wind Profiles From CESTM Rooftop



A lot going on here....

LiDAR Wind and CNR Time-height Cross Section at ASRC Roof, 05/28/2017



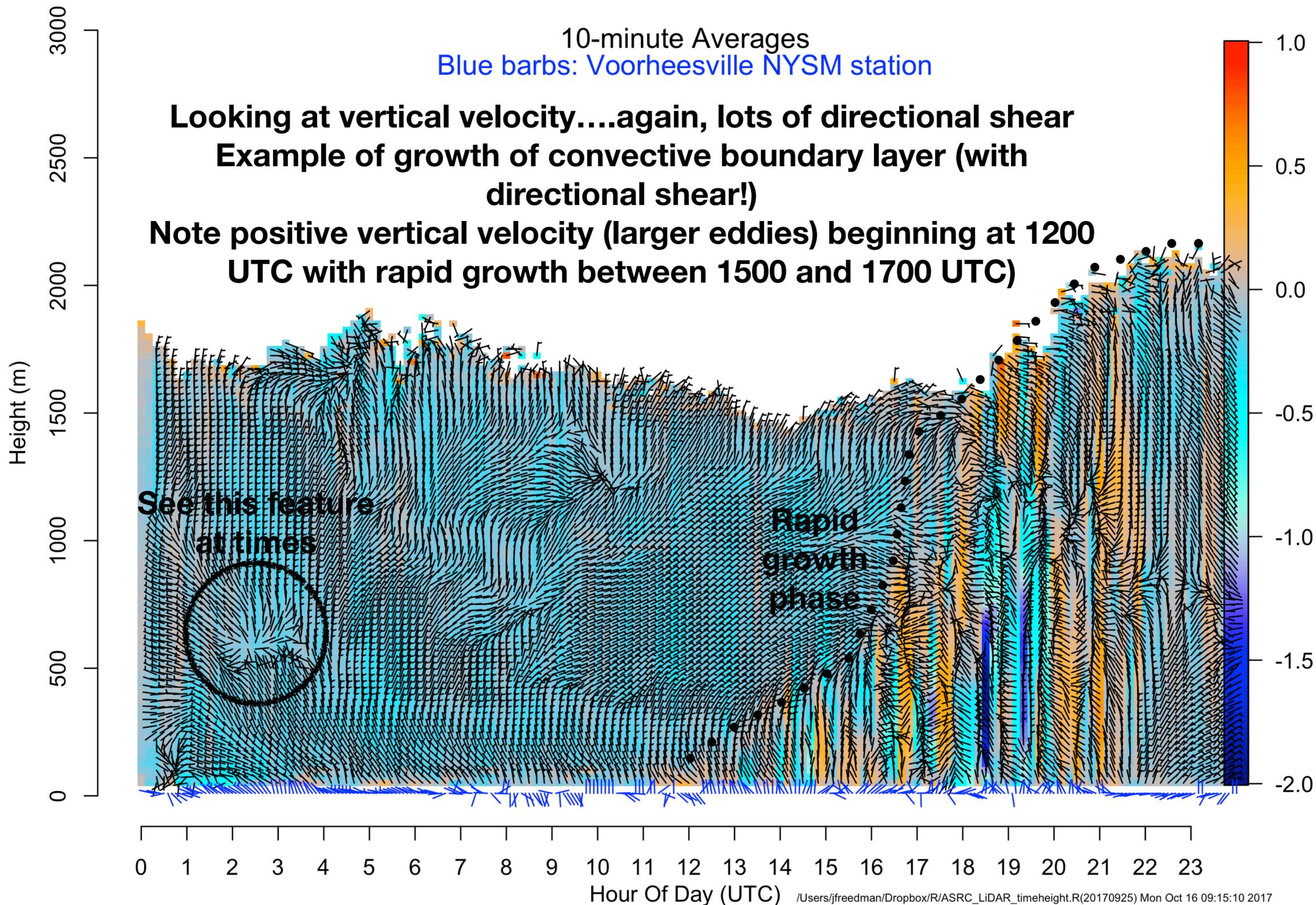
Light rain shower
between 0200 and
0300 UTC

CNR: carrier to noise ration (similar to SNR)

LiDAR Wind and Vertical Velocity Time-height Cross Section at ASRC Roof, 09/25/2017

One Full Wind Barb = 6 - 10 m/s

Filled Contours: Vertical Velocity (m/s)



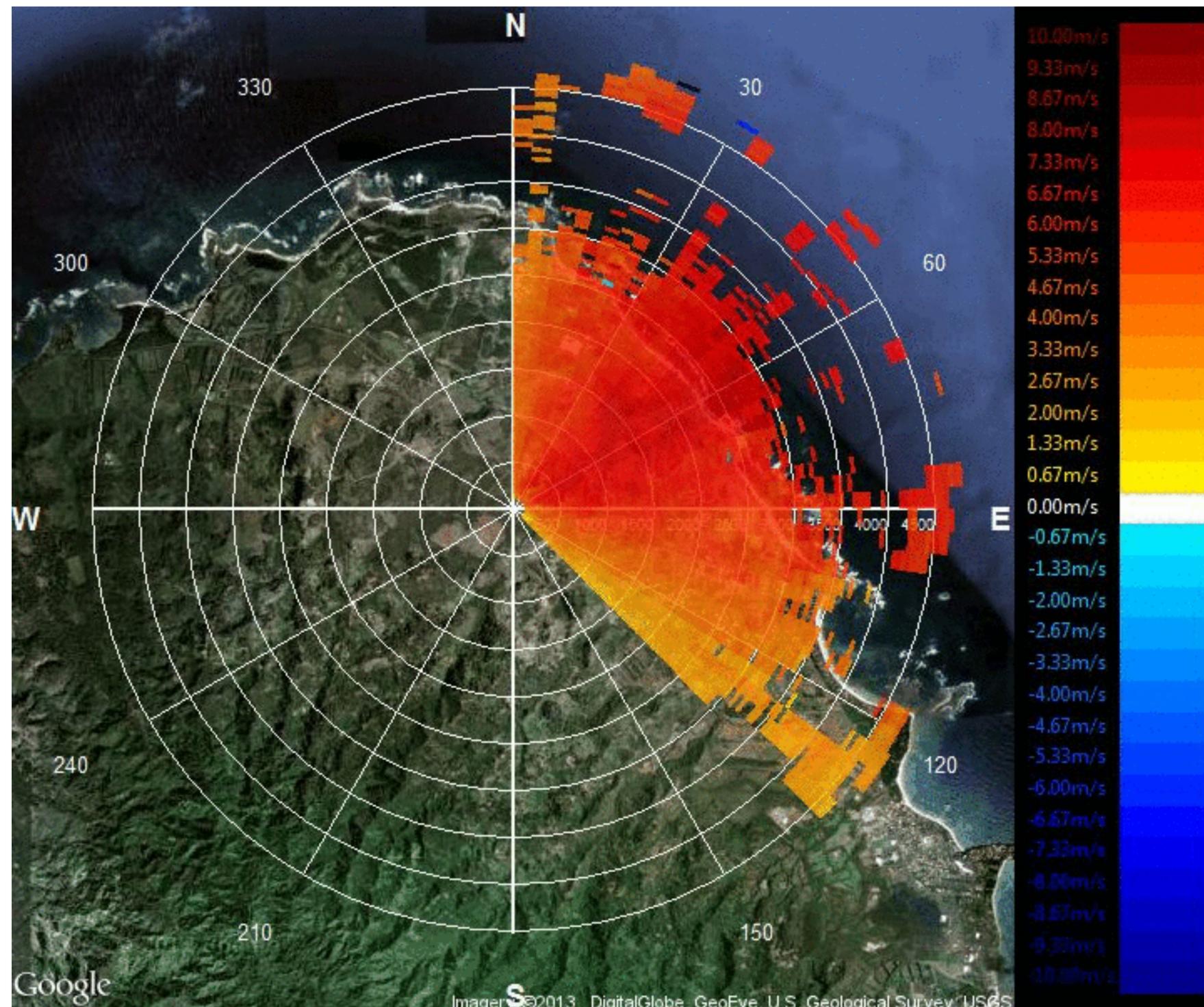
Leosphere Windcube 100S at Kahuku, Oahu

28 August 2013 0900 - 1500 UTC
Elevation angle = 10°

Disruption of Trade Winds

Persistent ENE winds
(towards LiDAR—
warmer shading)

Become more N, NW
flow (away from LiDAR
—cooler colors)



Next Class (Monday 2/6 – Lecture 5)

Offshore Wind and the Marine Atmospheric Boundary Layer (air-sea interactions)

Homework #1 DUE!!!

Zoom office hours (10 - 11:30 AM Monday)